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# NASA TECHNICAL MEMORANDUM

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## ATMOSPHERIC ENVIRONMENT FOR SPACE SHUTTLE (STS-2) LAUNCH

By D. L. Johnson and S. C. Brown Space Sciences Laboratory

December 1981

NASA



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#### TECHNICAL MEMORANDUM

## ATMOSPHERIC ENVIRONMENT FOR SPACE SHUTTLE (STS-2) LAUNCH

#### I. INTRODUCTION

This report presents an evaluation of the atmospheric environmental data taken during the launch of the Space Shuttle/STS-2 vehicle. This Space Shuttle vehicle was launched from Pad 39A at Kennedy Space Center (KSC), Florida, on a bearing of 60 degrees east of north at 1510 GMT (1010 EST) on November 12, 1981.

This report presents a summary of the atmospheric environment at launch time (L+0) of the STS-2, together with the sequence of prelaunch Jimsphere measured winds aloft profiles from L-13 h through liftoff. The gene all weather situation for the launch and flight area is described, and surface and upper level wind/thermodynamic observations near launch time are given. Surface and upper level wind/thermodynamic parameter measurements are also presented for the SRB descent/impact analyses.

Previous MSFC-related launch vehicle atmospheric environmental conditions have been published as Appendix A of individual MSFC Saturn Flight Evaluation Working Group reports [1]. Office memorandums have been issued for previous flights giving launch pad wind information. A report has also been published [2] which summarizes most launch atmospheric conditions observed for the past 155 MSFC/ABMA-related vehicle launches through SA-208 (Skylab 4). A report summarizing only STS-1 launch conditions is presented in Reference 3.

#### II. SOURCES OF DATA

Atmospheric observational data used in this report were taken from weather maps made by the National Weather Service, plus all available surface observations and measurements from around the launch area. Upper air observations were taken from balloon-released instruments sent aloft from Cape Canaveral Air Force Station (CCAFS) and from the ship Gen. H. S. Vandenberg in the Atlantic Ocean off the Florida Coast. High-altitude winds and thermodynamic data were measured by the Super Loki rocketsonde launched from the CCAFS. Table 1 presents a listing of systems used to obtain the upper level wind profiles used in compiling the final ascent meteorological data tape. Only the ship-launched Omegasonde-Rawinsonde and Super Loki rocket data were used in the upper level atmospheric regions for the construction of the final SRB descent/impact meteorological data tape. Data cutoff altitudes are also given in Table 1.

#### III. GENERAL SYNOPTIC SITUATION AT LAUNCH TIME

A high pressure ridge located west of Florida, oriented north-south throughout the east-central United States, began influencing the weather throughout Florida prior to and including launch time. The low-pressure storm system which had passed through Florida the preceding day was located in the Atlantic Ocean, east and north of Florida by launch time. Surface winds were moderate (27 ft/s) from the north northwest, with warm temperatures (73°F) being experienced in the KSC area. Figure 1 gives the surface weather map 3 hr prior to launch. Figure 2 presents the wind flow aloft at the 500 mb level. North to northwesterly winds dominated the flow aloft over the KSC region.

Cloud bands were located in the ocean areas surrounding the Florida peninsula, as shown in Figure 3. Figure 3 presents the GOES east (SMS-II) visible satellite picture taken an hour before launch (1400Z). Only scattered, low-level clouds were present in the KSC area during launch. Figure 4 shows the contrail of the Shuttle at launch as recorded by the GOES east satellites visible photograph taken at 1510Z. The directional change of the contrail was attributed to wind shear in the upper levels of the atmosphere.

#### IV. SURFACE OBSERVATIONS AT LAUNCH TIME

Surface observations at launch time for selected KSC locations are given in Table 2. Included are pad 39A, Shuttle runway, and CCAFS balloon release station observations. Neither precipitation nor lightning was observed at launch time.

Table 3 presents Pad 39A wind data along with other standard hourly meteorological measurements and sky observations for the 6 hr prior to launch of STS-2. Values for wind speed and direction are given for the 84 m (275 ft) FSS reference level and 18 m (60 ft) pad light pole level.

#### V. UPPER AIR MEASUREMENTS DURING LAUNCH

An estimated FPS-16 Jimsphere (L+0), GMD rawinsonde (1515Z), and Super-Loki rocketsonde (1710Z) systems were used to measure the upper level wind and thermodynamic parameters for STS-2 launch. At altitudes above the rocket-measured data, the Global Reference Atmosphere (GRA) [4] parameters for November KSC conditions were used. A tabulation of the STS-2 final meteorological data for ascent is presented in Table 4 which lists the wind and thermodynamic parameters versus altitude. A brief summary of parameters is given in the following paragraphs.

#### A. Wind Speed

At launch time, wind speeds were 27.0 ft/s (16.0 km) at 60 ft and increasing to a maximum of 158 ft/s (94.0 km) blowing from 286 degrees. This maximum occurred at an altitude of 36.300 ft (11.064 m). The winds decreased above this

level and then became stronger again at much higher levels, as shown in Figure 5. The overall maximum speed was 364.0 ft/s (216.0 km) at 200,000 ft (60,960 m) altitude.

#### B. Wind Direction

At launch time, the 60 ft wind direction was from the north northwest (345 degrees) and slowly shifted from the north to become westerly at approximately 39,000 ft (11,887 m). Wind directions stayed westerly up to 340,000 ft (103,632 m). Figure 5 shows the complete wind direction versus altitude profile. As shown in Figure 5, wind directions became quite variable at altitudes with low wind speeds.

#### C. Prelaunch/Launch Wind Profiles

All wind data, except L+0 values, shown in Figures 6 through 9 were measured by the Jimsphere FPS-16 system. All L+0 data are estimated.

The most unusual aspects of the wind profiles measured during the latter part of the countdown were the strong northerly winds in the lower 3,000 ft — a feature that persisted throughout the period — and the rapid wind speed increase at about 36,000 ft from L-3.5 hr to L+48 min. Changes in the wind profiles from L-13 to L-3.5 hr were relatively small — a decrease of maximum wind speed and slight veering of wind direction. However, between L-3.5 hr and L+48 min there was a large increase in wind speed at about 36,000 ft. This caused a large increase in the left crosswind component (Fig. 9).

After evaluating these rapid changes, it was decided that the L+48-min profile was not representative of the STS-2 ascent winds, and that a new profile more descriptive of the wind encountered during ascent was needed. The estimated L+0 wind profile was developed to satisfy that need.

#### D. Thermodynamic Data

The thermodynamic data taken at STS-2 launch time, consisting of atmospheric temperature, dew-point temperature, pressure, and density have been compiled as the STS-2 ascent meteorological data and are presented in Table 4. The associated thermodynamic data taken in support of the SRB descent have also been assembled as the STS-2 SRB descent/impact meteorological data and are presented in Table 5. The vertical structure of temperature for the STS-2 ascent and for the SRB descent is shown graphically versus altitude in Figure 10.

#### E. SRB Upper Air and Surface Measurements

As has been mentioned in earlier paragraphs, an SRB descent meteorological data tape has also been constructed which consists of data taken from the Omegasonde-Rawinsonde system (1728Z) aboard the USNS Vandenberg, which was stationed off the coast in the Atlantic Ocean. The CCAFS measured Super-Loki Rocketsonde data and the GRA model data were used at altitude levels above the measured

Omegasonde data. The tabular values for the SRB descent meteorological tape are presented in Table 5, with wind speed and direction profiles presented in Figure 11. Figure 10 gives the vertical temperature profile.

The surface-ship meteorological and oceanographical observations taken close to STS-2 SRB impact are presented in Table 6.

#### VI. ATMOSPHERIC SUMMARY CONDITIONS FOR STS LAUNCHES

Given in Table 7 are selected atmospheric T+0 launch conditions for all the Space Shuttle launches.

SYSTEMS USED TO MEASURE UPPER AIR WIND DATA FOR STS-2 ASCENT.\* TABLE 1.

			[	Portion of Data	Dataed	
	Release Time	Time	Start	t	End	
Type of Data	Time (UT) (h:min)	Time After L+0 (min)	Altitude m (ft)	Time After L+0 (min)	Altitude m (ft)	Time After L+0 (min)
FPS-16 Jimsphere**	15:58	48	4 (14)	87	17 069 (56 000)	106
Rawinsonde	15:15	ß	17 374 (57 000)	62	26 213 (86 000)	91
Super-Loki Rocketsonde	17:10	120	83 820 (275 000	120	27 432 (90 000)	110
Omegasonde-Rawinsonde*	17:28	138	18 (60)	138	29 870 (98 000)	236

\* The Omegasonde-Rawinsonde was released from the USNS Cen. H. S. Vandenberg to measure the upper atmosphere for SRB descent/impact analyses.

\*\* The T+17-min Jimsphere was unavailable. A second release at T+48 min provided Jimsphere wind data that was then used in the final meterological data tape, but was modified to reflect T+0 wind conditions.

TABLE 2. SURFACE OBSERVATIONS AT STS-2 LAUNCH TIME

								Sky Cover		puiM	Ð
Location	Time After L+0 (min)	Pressure, N/cm <sup>2</sup> (psia)	Temperature, K (°F)	Dew Point K (°F)	Relative Humidity (%)	Visibility km (miles)	Cloud Amount (Tenths)	Cloud Type	Height of Base Meters (ft)	Speed f/s (kn)	Direction (deg)
NASA Space Shuttle Runway	0	10.169	295.9 (73.0)	288.7	63	13	1	Strato- Cumulus	671 (2200)	15.2 (9.0)	320
Winds Measured at 10.4 m (34 ft)											
CCAFS <sup>d</sup> Surface Measurements	ĸ	10.169	295.6	289.1	19	,	,		,	25.0	310
		(14.75)	(72.0)	(61.0)						(14.8)	
Pud 39A lightpole NW 18.3 m	0	10.180	295. 9	288.2	61	1		,		27.0 <sup>C</sup> (16.0)	345°
(60.0 ก.)											
Pad 39A FSS (Top-NW) 83.8 m	0	,	•	ı	,	,	ı	,	1	27.0 <sup>c</sup>	355°
(275 ft)											

Pad 39A Camera Site 3 barometric pressure instrument appeared to be reading too high. Therefore, the KSC Shuttle runway station pressure of 10.166 N/cm<sup>2</sup> would be more appropriate as the L+0 pad atmospheric pressure measurement, to be applied at 21 ft above MSL.

b. Allitudes of measurements are above natural grade, except where noted.

c. I min average prior to L+0.

d. Bulloon release site.

e. Pad 39A thermodynamic measurements are taken at camera site =3, · 6.4 m (21 ft) above MSL.

\* Reduced to mean sea level, except PAD 39A observation.

and an analysis of

TABLE 3. STS-2 PRE-LAUNCH THROUGH LAUNCH KSC PAD 39A METEOROLOGICAL MEASUREMENTS\*

	=	Hourly Atmospheric		Measurements	nts				Sky	Sky Condition	
				275' Level (NW) **	e ve i	60' Level (NW) **	evel		Total		
12 November 1961 Time Z	Temp. (°F)	Dew Pt.	RH B	WS Kt	WD°	WS Kt	wD.º	Clouds	Sky Cover	Vis. (mi.)	Other Remarks
0.000	17.	ie Ie	¥%	23	340	2	270	1/10 CT at 2.000 ft	1/10	92	
1000	6	63	<b>36</b>	21	320	22	286	1/10 Ct' at 2,000 ft	17.10	2	
90:1	69	63	ã	23	350	8.	300	1/10 CU at 2.000 it	1/10	9	
1200	69	09	ε:	23	350	Ļ	320	1/10 CU at 1.800 ft	1/10	**	
1300	89	19	6-	7	300	1,2	270	1/10 CV at 1.800 ft	1 10	<b>a</b> o	
00+1	<u>ئ</u>	3	<u>:</u> -	12	290	13	280	1/10 CV at 2.000 ft	01/1	æ	
1500	73	59	63	17	340	91	320	2/10 SC at 2,200 ft	2/10	*	
16-**1510	7.3	59	19	91	355	9(	345	1/10 SC at 2,200 ft	1/10	*	
						-					

thurty verbal observations from CCAFS

.. 10 ain nean from instrumentation on NN side of pad 39A. Hourly verbal estimates from CCAFS.

1.0 PAD Wind and thermodynamic parameters obtained from KSC strip charts (\* 1 min average before L+0). FAD 39A L+0 Atmospheric Pressure, at 21 tt (MSL) was 10.166 N cm<sup>2</sup>.

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TABLE 4. STS-2 FINAL T+0 ASCENT METEOROLOGICAL DATA TAPE

ALI 11 UDE	•	WI ID DIRECTION	2	PRESSURE	NSIT	0
	(+1/SEC)	105.5	(DEG C)	(MILLIBARS)	Z :	(056 C)
	0.55	320	22-4	.1017+04	*D+1611.	15.0
00 10 00	027	347	22.1	. 101 4 • 04	* II 89+U4	6 · * **
00 00 00	026	350	21.7	1010+04	.1186+04	14.0
000300	027	355	21.3		·1184+04	14.7
0004000	010	054	20.9	-	42183408	
000200	032	900	20.5	• •	0	5.5
_	035	80 am	20.1	-	-1175+04	****
000700	037	545	10.1		40+411	
00000		) (F	F 0	•	1171+04	6.4
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001100	600	160	7.81		*D*6917*	A . C . C
	100	100	9-1-1	9	*D+D911.	
001100	0.33	359	17.5	18	.1158+04	13.7
00 14 00	031	003	•	.9684.03	.1155+04	# M • 6
001200	033	100	16.9	.9649+03	.1152+04	5.81
0	0.32	. 005		.9615+03	.1149+04	F
001700	# F O		16.2	=		
00 14 00				•	7000	7
	660	300	•		******	7.58
٠.	620	500	•	213	*0+1*11.	13.1
00 20 00	028	354	15.2	.9479+03	.1138+04	13.0
00 17 00	030	000	15.0	.9445+03	•1135+04	12.9
0	031	359	14.8	.9411+03	.11 32+04	12.1
00 22 00	033	003	14.6	.9378+03	.1129+04	12.6
00 24 00	035	003	****	.9344+03	.1125+04	12.4
00 25 00	0.35	500	16.2	-	1122+08	
00 26 00	032			"		
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00 53 00	920	013	13.4	.9177+03	•1109•0¢	11.7
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00100	025	031	12.1	_	.1071+64	-2.4
00 25 00	620	920	12.1	\$2	.1067+04	-2.5
004300		026	12.0	.8723+03	•1063+04	-2.6
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TABLE 4. (Continued)

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(FT)	•	(DEG)	(DEG C)	(MILLIBARS)	(GR AM/H 3)	(DEG C)
00 20 00		700		*	.1038+04	-3.4
02100	023	001	11.5	.8473+03	.1035+04	- N-
005200	023	100	11.3	.8442+03	.10 32+04	13.8
005300	021	<b>♦00</b>	11.0	12	.1029+04	
00 24 00	019	100	10.8	1	.1026+04	
00 55 00	076	466	10.6		.1023+04	-3.2
00 26 00	017	354	4.04	_	.1020+04	
005700	015	357	10.2	.8290+03	.1017+04	-3.2
00 58 00	0.18	345	6.6	.8259+03	.1014+04	-3.2
00 65 00	019	342	9.1	0	.1011+04	'n
00090	017	346	9.6	.8199+03	.1000+04	-3.1
006100	016	341	M • 6	.8169+03	.1005+04	-3.4
00 62 00	010	332	9.1	.6139+03	.1002+04	-3.7
36300	0	338	Ø • Ø	. 8109+03	.9996.03	0.4-0
064 GD	018	330	8.7	.8079+03	.9967+03	-4.3
00 65 00	019	333	8.8	. 0	,99 38+D3	9.4-
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74 00	019	348	9.9	~	_	9-
00 15 00	019	357	2.99	∞ .	•	1.7
76.00	910	349	9.0	•	<b>7</b>	b*/-
00 11 00	019	M and a	<b>2.</b>	-	5	-7.6
7800	020	351	6.3	.7672+03	5	-1.0
79 00	019	357	6.1	.7644.03	.9518+03	0.0.
0000	210	353	0.9	.7615+03	. 0+88+0.	-8.2
00 19 00	018	350	0.9	.7587+03	.9453+03	1.6-
8200	018	356	6.1	.7559+03	.9417+03	6.6-
00 63 00	016	*00	6.1	.7531+03	.9382+03	-10.8
00 84 00	010	000	6.2	.7503+03	.9346+03	-11.7
00 88 00	016	100	2-9	.7475+03	.9311+03	-12.5
00 96 00	019	010	2.9	•	.9276+03	-13.4
00 67 00	010	013	6.3	.7420+03	.9241+03	•
88 00	024	005	6.3	.7392+03	. 92 06+03	-18.2
00 68 00	027	900	6.4	•7365+03	.9171+03	•
00 06 00	026	900	**9	. 7338+03	.9136+03	-16.9
19100	026	005		.7311+03	. 9105+03	-17.º
00 92 00	027	358	6.2	.7283+03	907	
2	010	354	6.2	.7256+03	.9043+03	-17.2
00 20 00	120	355	1.9	.7230+03	.9012+03	
00 95 00	11.0	353	0.9	. 7203-03	.8981+03	-17.5
00 26 00	030	350	5.9	.7176+03	.8951+03	-17.4
00 97 00	0.32	048	<b>80 4</b> 0	•	. 89 20+03	-17.5
00 86 00	032	353	5.8	.7123+03	100 00 cm	-17.A

TABLE 4. (Continued)

GENSITY DEW POI	64 AH/H3) (DEG	8799+03	48-	740+03	711+03	681+03 -18	0.7	81-	81-	# 01 - 10 - 10 - 10 - 10 - 10 - 10 - 10		0 0 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	455+03	3	1-		A STORY	100 to 10		E0+54	1-222+03	199403	7070 - 120 -	NO+181	106+03	80+98	-6063+03		MO+400	1+03	-22			S-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0	35+03 -23	12+0	£2-	15.0 MO+	10403		50+04
PRESSURE	.7070+03	7044	•	-	ŝ	Φ.	*		6562+03	.40637403		•	.6735+03	,6710+03	*66.5 +03	*D+D800*	.6610+03	•	-	•	-6512+03	-	) eq	1	0	•	.6342+03	6294	. 0	-0	•6223•03	. 6174-03	.6152+03	.6129+03	50	.6082+03	ъ,	•	20. A 20	9K 7	•
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WIND SPEED (FT/SEC)	•	033	032		030		0.0	200	0.29	021	027	026	920	020	020	029	0.30	031	050		020	030	030	031	020	350	032	##O	032	032	031	032	031	030	034	0.30	6 P C	040	037	980	
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TABLE 4. (Continued)

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67 CI         CHO         CHO </td <td>01 67 50 01 89 50 01 89 00 01 90 50 01 92 00 01 93 00</td> <td>0.38</td> <td>311</td> <td>6.81</td> <td>.5081+03</td> <td>26</td> <td>~</td>	01 67 50 01 89 50 01 89 00 01 90 50 01 92 00 01 93 00	0.38	311	6.81	.5081+03	26	~
89 CD         67 68 + 03         + 67 68 + 03         + 52 2 1 + 03         + 67 68 + 03         + 53 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	01 89 00 01 90 00 01 90 00 01 92 00 01 93 00	0.0	308	-14.2	. 506 1 +03	6	*
89 CD         CD 37         305         -19.6         -5021-03         -6764-03         -19.8           90 CD         038         304         -15.3         -8081-03         -6764-03         -13.8           91 CD         039         304         -15.3         -8961-03         -677-03         -838           92 CD         037         302         -15.7         -8961-03         -6683-03         -38           94 CD         039         302         -15.7         -8961-03         -6683-03         -38           95 CD         040         299         -16.0         -8621-03         -663603         -38           95 CD         040         299         -16.2         -8681-03         -663603         -38           95 CD         040         299         -16.2         -8681-03         -663903         -38           95 CD         040         299         -16.4         -8621-03         -6639-03         -38           95 CD         041         301         -16.6         -8623-03         -6596-03         -38           96 CD         042         -8623-03         -6639-03         -38         -38           97 CD         048         -862-03	01 90 00 01 90 00 01 41 00 01 92 00 01 93 00	030	\$0£	-14.5	.5041+03	98+0	~
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4100         036         -15.3         4961+03         -6727403         -33           9200         037         302         -15.5         ,4961+03         -6683+03         -34           9200         039         302         -15.7         ,4961+03         -6683+03         -34           9400         039         303         -15.9         ,4961+03         -6683+03         -34           9500         040         299         -16.0         ,4861+03         -6639+03         -36           9500         040         299         -16.2         ,4861+03         -6596+03         -34           9500         040         300         -16.6         ,4862+03         -6596+03         -34           9500         045         301         -16.6         ,4823+03         -6574+03         -34           9500         045         304         -16.6         ,4823+03         -6574+03         -34	014100	0.00	#OM	-15-1	-	.6749+03	33
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690	-24.9	201000	.5770+03	
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	0.62-	10+4 5hm	-	-62.1
010	-25.9		. 56 99 40 3	
	-26.2	70.050	5663+03	,
	496-	7	3	- 2 5-
		**************************************		77
	4.02-	:0	20,000	-63.0
071		PO C PO P	. 56 33+0.3	
	-27.5	50.77.65	\$617.03	• • • • • • • • • • • • • • • • • • • •
	,	.3956+03		
		1010101		7
	-58.5	FO + C + C + C + C + C + C + C + C + C +	. 55.84 + 0.3	
		.3922.	•	
700				

TABLE 4. (Continued)

7	() 930)	8°5 *-	0.44-	-14.2	E. 4.	5.14-	1.11	6.4.	-45.1	-45.2		45.6	1.54-	-45.9	•	-46.2	E-94-	5.94-	9.94-	1.91	0.07	11/2		7.4		9.41-	1.81-	2.00-		9			10	•	5.64-	1.60-	•	ò	0	•	6		5 6	•		•	•
7 2	(GRAN/H3)	.5568+03	.5.48+03	.5329+03		£0+06 <b>*</b> 5 *	.5471+03	.5452+03	.54 33+03	.5413+03	.5394+03	.5376+03	.5357+03	.5339+03	.5321+03	.5302+03	284	99	*	. 52 30+0 3	.5213+03	£0+6416+	00+00 FM	1 =	12	Ó	. 50 88+03	.5071+03	.5053+03	. 5036+03	50.4106.	50-1006	•	W 0+84 64.	* 49 30+03	.4912+03	•	18	60+0	e i	26+0		50+26/4	50000000000000000000000000000000000000	9	47.25+03	
PRESSURE	(MILLIBARS)	.3906.03	.3889+03	387	.3856+03	0	.3824+03	. 380 7 +03	.3791+03		.3759+03	~	27	.3711+03	s.	. 1679+03		<b>6</b> 0	32	617+0	5	50+0005	<b>3</b> 4	9	524	509		.3479+03	94.0	- 1	•	1 5	1 1 0 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0	• 3375 + D3	.3360+03	5	-	0 + 9 1	302	•	2 :	9	ED+ # 175 *	2 -	D N	-	•
	(DEG C)	_	-29.0	-29.2	-29.3	-29.5	-29.1	-29.9	-30.1	-30.2	-30.4	-30.6	-30.8	-31.0	-31.2	m	m (	<b>M</b>	<b>m</b> 1	32	32 1	12.0	2 2	2 1	-	-33.7	-34.0	-34.2	-34.4	-34.6	0 C	0 * W * 1	35.0	-35.6	-35.7	-35.9	-36.1	-36.3	10 ° 9 ° 1	-36-7	-36.9		0 0 C F C		-38.0		
MIND DIRECTOR	(0EG)	297	297	298	300	299	298	298	29.7	299	298	300	300	300	301	300	565	268	662	962	293	204	206	294	296	203	967	295	568	292	700	20.5	294	294	295	295	295	295	294	# 6 C	* 60° C	166	292	200	292	293	
	(FT/SEC)		073	076	076	076	010	. 070	640	090	080	010	019	0.82	# # D	083	180	790	280	080	7 # 6 E	200		065	590	990	980	980	980	\	* et c	9 S	990	060	160	0.63	# 6D	096	E * 60	940			301	102	103	104	
300 11 17	(£1)	02 50 00	3	2	02 53 00	3	02 55 00	8	025760	02 58 00	05 25 00	00 09 20	02 61 00	02 62 00	026300	00 69 20	02 55 00	07.00	00,420	00 00 00	00.49.70	02.17.00	02 72 00	02 73 00	02 74 00	02 75 CO	02 76 00	027760	02 78 C 0	006/20	020100	02 82 00	028300	02 84 00	028500	02 96 00	02.87.00	02 88 20	02.69.00	0000	024700	029100		02.95.00	05 96 00	97	00000

TABLE 4. (Continued)

100   100	(F T)	WIND SPEED	WIND DIRECTION	TEMPERATURE	20174		
100   272   19,0   19	03000	?:	(DEC)	(DEG C)	TENEST TENEST	MSIT	DEN POI
10	030100	110	292	0.00	104 4 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	E/E/	
100   20   20   20   20   20   20   20	030200		291	-38.9	10.00 E	0+0	-51
100   272   275	! "	101	291	-39.1	- 12 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	58+0	N
100   201	03.04.00	) d	291	-39.2	.3104-03	7 7 7 7	N ::
11	03 05 00	100	162	-39.4			м.
10	030600		292	-39.5	.3077+03		-52.3
11	030700	112	667	-39.6	. 306 3+03	100 - 00 - 00 - 00 - 00 - 00 - 00 - 00	.25-
11	030800	) P 01	562	-39.8	105050		-25-
11	030900	116	295	•	3036+04	50+36 54 ·	-52
11	031000	- P - P - P - P - P - P - P - P - P - P	162	2	. 302 3+03	20.00.00	-52.
11	031100	111	662	0	1000ET	50×10×4	-52.9
11	031260	9 * •	295	0	2006 401	50+00 65	~
10	031300	777	162	0	1041 405	50+00+++	-53.2
12	031400	- 12	295	-40.0	100 to 100 to 1	0.0	
12	031500	277	297	-41.2	295 6 + OT	0.00	-53.
120   294   -41.7   -291.03   -191	031600	D ( )	962	-	204 1 00		-53.
120   294   42.2   289   43   43   43   43   43   43   43   4	031700	118	295	•	2010105	24+0	-53.
120   294   42.2   294   41.5   10.5   13.0   10.5   10.		121	<b>*62</b> .	0 1 4	F	0 * * 0	-54.
120	2001	120	762	6.64*	£0.1742.	.4394+03	-54.
120		611	294	4.64	-can4+03		
120   295   42.9   286.5.03   43.36.03   45.36.03   4	00000	121	294		EO+1697*	• 4365+03	
121   293	001750	120	295	-42.0		• 43 50+03	•
121   222   222   43.5   43.5   43.60.3   43.06.03	20 27 20	123	293		· 6465+U3	. 43 34+03	6.984
122   291	0324.20	121	293	) M	50.76920	.4316+D3	80
122   291   -43.9   -2813.03   -425.03   -45.9   -45	0125.00	777	292		FD- 4 C B Y .		-
121   221   48.5   276   603   42 (10.0 )   45 (10.0 )	00000	521 ·	291	-63.7	50+9787	•	-53.
120	00000	122	291	0 7 4 1	50+519+0	~	35
120   292   422603		121	291	-84.1	-11	so.	55
12	0120 CB	120	292		в.	.4240+03	
122   290   44.6   2751.403   4176.03   45.6   25.6   290   4176.03   4176		617	290			~	-56-
122   290	00000	121	290	F - M -	η.		36
123         200         95.0         2726-03         4179-03         -85.0           123         209         -45.4         -2701-03         4145-03         -85.0           127         209         -45.4         -2701-03         4145-03         -85.0           127         209         -45.4         -2701-03         4145-03         -85.0           129         209         -45.4         -2604-03         -413-03         -87.0           130         209         -45.4         -2607-03         -4000-03         -87.0           130         207         -45.4         -2607-03         -4000-03         -87.0           130         207         -46.0         -2607-03         -4000-03         -87.1           130         207         -46.0         -2608-03         -4000-03         -8000-03           130         208         -46.0         -2608-03         -4000-03         -8000-03           130         208         -46.0         -2608-03         -4000-03         -8000-03         -8000-03         -8000-03         -8000-03         -8000-03         -8000-03         -8000-03         -8000-03         -8000-03         -8000-03         -8000-03         -8000-03         -8000		221	290		• (	.4194+03	5
123     269     -45.3     -2713403     -4161403     -56.5       127     267     -45.3     -2713403     -4169403     -51.2       128     267     -45.3     -2713403     -4169403     -57.3       129     286     -45.4     -268403     -413403     -57.3       130     286     -45.4     -268403     -406403     -57.4       130     287     -46.0     -268403     -406403     -57.4       130     287     -46.0     -268403     -408403     -57.4       130     287     -46.0     -26840403     -408303     -57.4       130     287     -46.0     -26840403     -408303     -57.4       130     286     -46.0     -26840403     -408303     -57.4       130     286     -46.0     -26840403     -408303     -57.4       130     286     -46.0     -26840403     -408403     -408403       130     286     -46.0     -26840403     -408403     -58.4       130     286     -46.0     -26940403     -408403     -58.4       130     286     -46.0     -26940403     -36940403     -408403       131     286     -46.0     -26940403 <td>22.50</td> <td>122</td> <td>290</td> <td>•</td> <td>ю,</td> <td>-4178+03</td> <td>36.</td>	22.50	122	290	•	ю,	-4178+03	36.
123     290     -45.3     -2713.403     -4145.03     -4145.03     -45.9003     -57.2001       120     287     -45.9     2664.03     -406.03     -406.03     -57.2664.03       130     287     -46.0     -2664.03     -406.03     -57.2001       130     287     -46.0     -2664.03     -4064.03     -57.2001       130     287     -46.0     -2664.03     -4064.03     -57.2001       130     287     -46.0     -2622.03     -4064.03     -57.2001       130     287     -46.0     -2622.03     -4064.03     -57.2001       130     285     -46.0     -2624.03     -4018.03     -58.2       130     285     -46.0     -2604.03     -4018.03     -58.2       130     285     -46.0     -2604.03     -8018.03     -8018.03       130     285     -46.0     -2604.03     -8018.03     -8018.03       131     285     -46.0     -2604.03     -8018.03     -8018.03       141     285     -47.0     -2604.03     -8018.03     -8018.03       141     285     -4018.03     -8018.03     -8018.03     -8018.03       141     285     -4018.03     -8018.03     -8018.03 <td>7</td> <td>123</td> <td>289</td> <td>1.5</td> <td>. 2726-03</td> <td>.4161.03</td> <td></td>	7	123	289	1.5	. 2726-03	.4161.03	
127     267     -45.4     -269.03     -4129.03     -57.       129     286     -45.5     -269.03     -406.03     -57.       130     287     -45.6     -45.03     -406.03     -57.       130     287     -46.0     -269.03     -406.03     -57.       130     287     -46.0     -269.03     -408.03     -57.       130     287     -46.1     -2616.03     -408.03     -57.       130     287     -46.3     -2616.03     -4018.03     -58.       130     285     -46.4     -2616.03     -4018.03     -58.       139     285     -46.4     -2616.03     -4018.03     -58.       139     285     -46.4     -2501.03     -3976.03     -80.       139     285     -47.8     -255.00     -3976.03     -80.       141     285     -47.8     -255.00     -3976.03     -80.0       141     285     -47.8     -255.00     -3976.03     -80.0       141     285     -47.8     -255.00     -255.00     -255.00       141     -47.8     -255.00     -255.00     -255.00     -255.00       141     -48.0     -255.00     -255.00     -255.00	)     	123	290		2713+03	.4145+03	
120     207       130     286       130     286       130     287       130     287       130     287       130     287       130     287       130     287       130     287       130     286       130     286       130     286       130     286       130     286       130     286       130     286       130     286       130     286       130     286       130     286       131     286       132     286       133     286       134     286       135     286       141     286       141     286       141     286       141     286       141     286       141     286       141     286       141     286       141     286       141     286       141     286       141     286       141     286       141     286       141     286       141     286		121	287	Y	21011	.4129.03	-
130 286 287 -45.0 287 -46.0 287 -46.0 287 -46.0 287 -46.0 287 -46.0 287 -46.0 287 -46.0 287 -46.0 287 -46.0 287 -46.0 287 -46.0 287 -46.0 287 -46.0 287 -46.0 287 -46.0 288 -46.0 288 -46.0 288 -46.0 288 -46.0 288 -46.0 288 -46.0 288 -46.0 288 -46.0 288 -46.0 288 -46.0 288 -46.0 288 -46.0 288 -46.0 288 -46.0 288 -46.0 288 -46.0 288 -46.0 288 -48.0 288 -48.0 288 -48.0 288 -48.0 288 -48.0 288 -48.0 288 -48.0 288 -48.0 288 -48.0 288 -48.0 288 -48.0 288 -48.0	00 20 00	128	287	, ,	£0+6897•	•4113+03	-57.1
129   287   -46.0   -268.0   -268.0   -268.0   -4080.0   -408.0   -408.0   -408.0   -408.0   -408.0   -408.0   -408.0   -408.0   -408.0   -408.0   -408.0   -258.0   -408.0   -258.0   -258.0   -258.0   -408.0   -258.0		0.1	286	•	2017103	₽	57.
130 207 4064-03 130 207 46-10 2640-03 4018-03 131 267 46-10 2616-03 4018-03 130 205 46-10 2604-03 4018-03 130 205 46-10 2604-03 4018-03 130 205 46-10 2604-03 3976-03 130 205 46-10 2650-03 3976-03 130 205 47-3 2650-03 3976-03 141 206 400-03 3920-03 142 205 405 505 143 205 405 3934-03 143 205 406-03 3920-03		129	207	•	50++907+	÷	-
133 287 -46.1 .2624.03 .4034.0			207		10-2507	0++9	2
133 267 -46.5 .2616.03 .40134.03 139 265 -46.6 .2692.03 .40104.03 139 265 -46.6 .2692.03 .3976.03 139 265 -40.8 .2691.03 .3976.03 139 265 -47.8 .2659.03 .3976.03 141 265 -47.8 .2657.03 .3976.03 142 265 -40.0 .2557.03 .3976.03 143 265 -40.0 .2557.03 .3920.03	2000	2.30	287	3	50+0+07+	0.0	57
350   266   266   2674   27   27   27   27   27   27   27			287	3		33+0	•
139 285 4004-03 4004-03 30004-03 30004-03 30004-03 30004-03 30004-03 30004-03 30004-03 30004-03 30004-03 30004-03 30004-03 30004-03 30004-03 30004-03 30004-03 30004-03 30004-03 30004-03 3004-03 30004-0	02.42.00	136	286	3		18+0	2
265 -47.2 .2554.03 .3976-03 .3		D (1)	205	Z	50++092+		-58.1
265 -47.5 .2569.03 .3940.03 265 -47.5 .2567.03 .3940.03 265 -47.6 .2565.03 .3934.03 266 -46.0 .2545.03 .3930.03 265 -46.3 .2557.03	0145.00	95.1	265	-47.1	258 : 404		-88.2
141 285 -47.6 .2557.03 .3940.03 .3940.03 .3940.03 .3940.03 .3940.03 .3940.03 .3940.03 .3940.03 .3940.03 .3950.00 3 .3950.00 3 .3950.00 3 .3950.00 3	03 64 00	77	205	-47.3	5440.00		-20.
141 285 -47.6 .2545-03 .3544-03 .3946-03 .2544-03 .2544-03 .2545-03 .2554-0	014700		285	2.4.		. 3962+03	-31.5
200 May 200 Ma		7 1	285	-47.8	256 6 404	MD+0+65.	-58.7
80 MD+02AP0			286	. 6.484.		50+056	-28.
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Colombia Filton

TABLE 4. (Continued)

\$13+66#C*	
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	-51.5
	-51.7
	-51.8
1	-52.0
	1.76-
	-52.4
!	-52.5
	-52.7
	-52.8
	-5 3. C
	-53.4
<b>1</b>	-53.6
į	-53.8
	-53.9
	-54.1
	-54.2
	-54.4
	-54.5
	-54.7
	-54.8
	-55.0
	-55.1
	-55.3
	-55.4
	-55.6

TABLE 4. (Continued)

17.0   10.0							
120	F1	FT/	(0£6)	U	(WILLIBARS)		401
120	0000	129	279	-25.9	.1986+03		
110	001040	129	277	-56.0	~	17	-65.
13	04 02 00	130	278	-56.1	~	.3157+03	99
11	040300	129	278	-56.2	58	. 31 43+03	-99-
111	00 40 40	132	278	-56.3	2	.3130+03	•
111	04 65 00	131	278	-56.3	8	.3116+03	?
13	04 06 00	131	278	-56.4	30	• 31 0 3+0 3	9
120	04 07 00	* F R	277	-56.5	21	.3089+03	Ť
130   100	00 00 00	129	277	-56.6	2	3076+03	99-
131   274   -56.8   -1869.103   -1015   -101	040900	130	275	-56.7	6	Ð	99-
120	000100		27%	-36.8	9	.3049+03	99-
126   127   128	04 11 00	129	273	-5.6.9		.3035+03	79
129   271   -57.0   -1856.03   -296	041200	128	273	6.95-	.1875-03	.3022+03	-67
122   277   -574	041300	129	27.1	57	.1866.03	.3008+03	7
126	04140	127	271	2	2	.2995+03	<b>-6</b> 7
132   272   274   275   276   1831 0	04 15 00	126	270	2		.2982-03	19-
132   272   274   1812   274   275   285	C4 16 CO	129	27.1	5.1	0	.2968+03	7
133   274   275   274   275	041700	132	272	-57.3	.1631+03	.2955+03	17
136   274   -57.5   1005-013       137	0.000	133	274	5	.1822-03	.2942+03	7
134   274   -57.6   1706.03   2.2   1.2   2.2   1.2   2.2   1.2   2.2   1.2   2.2   1.2   2.2   1.2   2.2   2.2   1.2   2.2	00 61 00	135	274	5	.1614-03	.2929+03	
137   274   -57.6   -1796-03   -2.5   -1796-03   -2.5	04 20 00	134	274	-57.5	. 1805+03	.2916+03	-
136   275   -57.6   -1799-01   -27	04 21 00	137	274	-	.1796+03	. 2902+03	7
139   275   -57.4   -1776.03   -286	04 22 0 0	<b>80</b> F	274		.1788+03	.2869+03	
190   275   -57.7   -1711-03   -286       180   277   -57.4   -1754-03   -286       180   277   -57.4   -1724-03   -286       180   277   -58.1   -1724-03   -286       181   277   -58.1   -1724-03   -275       182   277   -58.1   -1724-03   -275       183   277   -58.1   -1724-03   -275       184   277   -58.2   -1674-03   -275       185   277   -58.4   -1674-03   -275       186   277   -58.4   -1677-03   -268       186   277   -58.5   -1677-03   -268       186   277   -58.5   -1657-03   -268       186   277   -58.5   -1657-03   -268       187   277   -58.5   -1677-03   -268       188   277   -59.2   -1600-03   -258       189   277   -59.3   -1600-03   -258       180   277   -59.3   -1500-03   -258       180   277   -59.3   -1500-03   -258       180   277   -59.3   -1500-03   -258       180   277   -59.3   -1500-03   -258       180   277   -59.3   -1500-03   -258       180   277   -59.3   -1577-03   -258       180   277   -59.3   -1577-03   -258       180   277   -29.3   -29.3       180   277   -29.3       180   277   -29.3       180   277   -29.3       180   277   -29.3       180   277   -29.3       180   277   -29.3       180   277   -29.3       180   277   -29.3       180   277   -29.3	042350	139	275		1179+03	.2976+03	7
Second   S	042400	074	275		.1771+03	.2863+03	-67
25	042500	141	275	-57.7	.1762+03	.2850+03	99
27         -57.0         -1745-03         -28           27         -57.0         -1724-03         -27           2800         135         276         -58.0         -1724-03         -27           2800         135         277         -58.1         -1724-03         -27           3100         135         277         -58.1         -174-03         -27           3100         135         277         -58.1         -174-03         -27           3100         132         279         -58.1         -174-03         -27           3100         120         279         -58.3         -1679-03         -27           3100         120         279         -58.4         -1679-03         -27           3100         120         279         -58.5         -1677-03         -27           3100         120         275         -58.5         -1647-03         -28           3100         120         274         -58.6         -1647-03         -28           3100         120         274         -58.6         -1647-03         -28           3100         116         274         -58.6         -1647-03         -28	04 26 00	139	276	-57.8	.175#+03	.2837+03	9
200         136         278         -57.9         -1720-03         -279           200         135         277         -58.1         -1720-03         -279           3100         135         277         -58.1         -1720-03         -279           3100         135         279         -58.2         -150-03         -279           3100         130         279         -58.3         -150-03         -279           3100         126         279         -58.3         -150-03         -279           3100         126         279         -58.3         -1671-03         -272           3100         126         279         -58.3         -1671-03         -272           3100         126         277         -58.4         -1671-03         -272           3100         126         277         -58.4         -1647-03         -258           3100         136         277         -58.4         -1647-03         -268           310         136         278         -28.4         -1647-03         -268           310         136         278         -28.4         -1647-03         -268           310         136 <td>04 27 00</td> <td>828</td> <td>277</td> <td>-57.8</td> <td>.1745-03</td> <td>.2824+03</td> <td>-</td>	04 27 00	828	277	-57.8	.1745-03	.2824+03	-
29 CG         137         278         -57.9         -1728-03         -278           30 CG         135         277         -58.1         -172 CG         -278           31 CG         135         279         -58.2         -170 CG         -278           33 CG         137         279         -58.3         -170 CG         -278           33 CG         128         279         -58.3         -150 CG         -278           34 CG         128         279         -58.3         -150 CG         -278           35 CG         128         279         -58.3         -167 CG         -278           35 CG         128         -278         -167 CG         -278           36 CG         128         -167 CG         -278         -278           40 CG         128         -58.6         -167 CG         -268           40 CG         130         -278         -58.6         -167 CG         -268           40 CG         130         -278         -58.6         -167 CG         -268           40 CG         130         -278         -58.6         -167 CG         -168         -268           40 CG         130         -278	04 28 00	138	278	2	.1737+03	.2811+03	7
135   277   -58.1   1712-03   -277   -28.1   1712-03   -277   -28.1   1712-03   -277   -28.1   1712-03   -277   -28.1   1712-03   -277   -28.1   1712-03   -277   -28.3   -279   -28.3   -279   -273	04 29 60	137	278	-	.1728.03	.2798+03	•
31 00         135         277         -58.1         .1712.03         .279           32 00         133         279         -58.2         .1704.03         .274           33 00         130         279         -58.3         .1597.03         .273           35 00         120         277         -58.4         .1671.03         .275           35 00         126         277         -58.4         .1671.03         .275           37 00         126         277         -58.6         .1647.03         .275           37 00         126         277         -58.6         .1647.03         .26.8           39 00         136         277         -58.6         .1647.03         .26.8           30 00         136         277         -58.6         .165.4.03         .26.8           30 00         136         278         -58.6         .165.4.03         .26.8           31 00         136         278         -58.6         .165.4.03         .26.8           32 00         136         279         -58.9         .165.4.03         .26.8           32 00         162 00         .162 00         .162 00         .26.9           32 00	54 30 00	135	278	-58.0	.1720+03	.2785+03	9
120         133         279         -58.2         .1704.03         .274           134 00         132         279         -58.3         .1696.03         .273           134 00         130         279         -58.3         .167.03         .273           136 00         126         277         -58.4         .1677.03         .273           136 00         126         275         -58.5         .1647.03         .274           137 00         126         277         -58.6         .1647.03         .268           140 0         116         274         -58.6         .1647.03         .268           140 0         116         274         -58.6         .1647.03         .268           140 0         116         274         -58.6         .1647.03         .268           140 0         116         274         -58.6         .1647.03         .268           150 0         116         276         -58.9         .1647.03         .268           150 0         116         276         -58.9         .1647.03         .268           150 0         116         277         -59.0         .1647.03         .261           150 0<	04 31 00	135	277	-58.1	.1712-03	.2773+03	-69-
33 LO         132         279         -58.2         -1696-603         -273           13 LO         279         -58.3         -1587-03         -273           13 LO         276         -58.3         -1679-03         -273           15 LO         277         -58.4         -1679-03         -273           15 LO         277         -58.5         -1647-03         -276           16 LO         122         274         -58.6         -1647-03         -269           16 LO         13         274         -58.6         -1647-03         -269           16 LO         13         279         -58.6         -1647-03         -269           16 LO         13         276         -58.9         -1647-03         -269           16 LO         13         279         -58.9         -1647-03         -269           16 LO         13         279         -59.2         -1647-03	04 32 00	133	279	-58.1		42760+03	
34 CO     130     279     -58.3     -157.03     -273       35 CO     129     276     -58.4     -1677.03     -275       37 CO     126     277     -58.4     -1677.03     -275       37 CO     126     277     -58.6     -1677.03     -26.9       39 CO     122     277     -58.6     -1647.03     -26.9       39 CO     130     277     -58.6     -1647.03     -26.9       42 CO     136     277     -58.6     -1647.03     -26.9       42 CO     136     279     -58.9     -1639.03     -26.9       42 CO     136     279     -58.9     -1639.03     -26.9       45 CO     13     279     -58.9     -1639.03     -26.9       45 CO     13     279     -59.0     -1624.03     -26.9       45 CO     13     279     -59.0     -1624.03     -26.0       46 CO     13     279     -59.0     -1624.03     -26.0       45 CO     13     279     -59.0     -1624.03     -26.0       46 CO     13     279     -59.0     -1624.03     -26.0       46 CO     16     16     -16     -26.0     -26.0 <t< td=""><td>3</td><td>132</td><td>279</td><td>-58.2</td><td>•</td><td>.2748+03</td><td>89-</td></t<>	3	132	279	-58.2	•	.2748+03	89-
35 00     129     278     -58.4     -1671.03     -272       36 00     126     275     -58.4     -1671.03     -273       37 00     122     275     -58.6     -1643.03     -269       39 00     122     276     -58.6     -1647.03     -269       39 00     122     277     -58.6     -1647.03     -269       40 00     116     277     -58.6     -1637.03     -269       42 00     116     279     -58.6     -1637.03     -269       45 00     116     279     -58.6     -1637.03     -269       45 00     118     279     -58.6     -1616.03     -269       46 00     118     279     -58.6     -1608.03     -261       46 00     118     279     -58.0     -1608.03     -261       46 00     118     279     -58.0     -1608.03     -261       47 00     118     279     -58.0     -1608.03     -261       48 00     118     279     -58.0     -1608.03     -261       48 00     118     279     -58.0     -1608.03     -261       48 00     118     279     -58.0     -1608.03     -261       <	2	130	279	-58·3	~	.2736+03	89-
126     277     -58.4     -1671.403     -271       3700     126     275     -58.5     -1653.05     -259.5       3700     122     276     -58.6     -1655.03     -269.5       3700     122     277     -58.6     -1657.03     -269.5       3900     116     277     -58.6     -1657.03     -269.5       4200     116     278     -58.9     -1657.03     -269.4       4200     116     278     -58.9     -1608.03     -265.4       4500     118     279     -59.0     -1616.03     -261.0       4500     118     279     -59.0     -1616.03     -261.0       4500     118     279     -59.0     -1608.03     -261.0       4500     118     279     -59.0     -1608.03     -261.0       4500     118     279     -59.0     -1608.03     -261.0       4500     118     279     -59.0     -1608.03     -261.0       4500     118     279     -59.0     -1608.03     -261.0       4500     118     279     -289.3     -1608.03     -261.0       4500     118     279     -289.3     -1608.03     -261.0 <t< td=""><td>04 35 00</td><td>129</td><td>278</td><td>-58.3</td><td>•</td><td>.2723+03</td><td>9</td></t<>	04 35 00	129	278	-58.3	•	.2723+03	9
37 CQ     126     275     -58.6     .1655.03     .269       19 CQ     122     276     -58.6     .1647.03     .269       39 CQ     116     277     -58.6     .1647.03     .265       42 CQ     116     274     -58.6     .1631.03     .265       42 CQ     116     279     -58.9     .1624.03     .265       44 CQ     116     279     -58.9     .1616.03     .265       45 CQ     116     279     -59.0     .1616.03     .261       45 CQ     116     279     -59.0     .1616.03     .261       46 CQ     116     277     -59.1     .1600.03     .261       46 CQ     116     274     -59.2     .1600.03     .251       47 CQ     116     274     -59.2     .1502.03     .254       48 CQ     116     274     -59.2     .1502.03     .255       48 CQ     116     277     -59.2     .1502.03     .255	04 36 CO	126	27.7	-58.4	-	.2711+03	40
1900 122 276 -56.6 .1655.03 .268 .269 .269.0 .1647.03 .268 .269 .264 .279 .286 .286 .274 .286 .286 .286 .286 .286 .286 .286 .286	04 37 00	126	275	-58.5	3	.2699.03	7
19 00         12 0         27 7         -56.6         .1647.03         -26 75           40 00         116         274         -56.7         .1639.03         .265.1           42 00         116         277         -56.9         .1624.03         .265.1           42 00         116         278         -59.0         .1624.03         .265.1           45 00         118         279         -59.0         .1600.03         .265.0           45 00         118         277         -59.1         .1600.03         .26.16           46 00         118         277         -59.2         .1600.03         .26.03           46 00         118         277         -59.2         .1592.03         .25.63           46 00         110         110         277         -59.2         .1592.03         .25.93           46 00         110         277         -59.2         .1592.03         .25.59	00 01 00	122	276	20	.1655+03	.2687+03	9-
42 00 119 274 -56.7 1639+03 -2665 110 110 277 -56.9 1631+03 -2665 110 277 -56.9 1631+03 -2651 110 278 -56.9 1624+03 -2624 130 -2640 130 -2624 130 -2624 130 -2624 130 -2624 130 -2624 130 -2634 130	04 39 00	120	27.7	-58.6	. 1647+03	75	9
110 116 277 -58.8 .1631.03 .2651 120 116 278 -58.9 .1624.03 .2640 130 119 279 -59.1 .1608.03 .2658 1400 119 277 -59.1 .1600.03 .2603 1400 115 274 -59.1 .1600.03 .2603 1400 110 271 -59.1 .1662.03 .2563	0000	617	274	-58.1	.1639+03	3	
4200 116 278 -56.9 .1624.03 .26.90 4200 12.00.00 12.00.00 12	00 11 00	116	277	-58·B	.1631+03	.2651+03	666-
4300 114 276 -59.0 .1616.03 .262 4400 115 277 -59.1 .1608.03 .261 4700 115 274 -59.2 .1559.2-03 .256 4800 115 274 -59.4 .1559.2-03 .256 4800 110 271 -59.4 .1577.03 .257	04 42 00	116	278	5.8	.1624.03	.2640+03	0000-
44 00 113 277 -59.1 .1600.03 .26 0 .	7	# ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) (	278	20	. 1616+03	Ň.	6666
4500 114 277 -59.2 .1500.403 .25 4600 115 274 -59.2 .1592.403 .25 4700 110 275 -59.4 .1577.03 .25	:	113	279	-20.1	.1605-03		
46.00 115 274 -59.2 .1592.03 .25 47.00 - 110 275 -59.3 .1585.03 .25 48.00 110 271 -59.4 .1577.403 .25	Ş	***	211	1.05-	.1600+03	•	
4750 . 110 . 275 - 594.9 . 1585.03	;	91 T	274	N-65-	NI	ED+5457	
20 10+1/51" 0:05" 1/2 CIN 100"	~	011	275	2	•	5D+2862*	6.6
	5		226	4.07	۰	7	֓֓֜֝֓֜֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֜֓֓֓֓֓֓֡֓֓֡֓֜֓֡֓֡֓֜֓֡֓֡֓֜֡֓֡֓֡֓֜֡֓֡֓֜֡֓֡֓֡֓֜֡֡֓֡֡

TABLE 4. (Continued)

METEOROLOGICAL DATA	IAPE	MOTTO CATA	1 5 mp FD AT 110 F	90f C4110f	OF NSITY	DEW POINT
(11)	IFT/SEC)	(DEG)	(DEG 1)	(MILLIBARS)	•	EG
	101	27.1	1051	1562+01	.2548+03	-6666-
		1 0	٠.		, ,	
001640	0 1	0/2			50.05.57	90001
20 25 60	707	407	1946	• 1	50×6267•	**************************************
04 53 00	101	268	-59.8	.1539+03	.2513+03	- 4666-
00 45 40	108	267	-89.8	.1532+03	.2502+03	-6666-
04 55 00	808	265	-59.9	.1525+03	.24 90+03	-6666-
00 99 00	107	266	-60.0	.1517+03	.2479+03	-6666-
04 57 00	100	265	0-09-	.1510+03	.2468+03	-6666-
04 54 00	109	264	-60.1	.1502+03	.2457+03	-6666-
09860	112	262	-60.1	1495+03		.0666-
0009#0	MET	26.0	-60.2	10+8841	2434+03	-6666-
046100	112	200	-60.2	-	2423403	-9999
046200	611	25.6			.2412+03	-6666-
00.54.00	411	246	F - 09 -	2	2011-03	6666-
	9	9 40	4 04		F C + C 0 F C	0000
00 49 40	2 7 7	107		) i	50.04.57	n i e
00000	10 F	797		,	5014/57	• • • • • • • • • • • • • • • • • • • •
00 00 00	717	504	C • D 9-	50. C. b. 1	•	
046700	121	262	-60.5	.1438+03	.2357+03	- 66 66-
04 68 C0	122	264	9.09-	.1431+03	.2346+03	-6666-
00 69 60	123	261	. 9.09-	.1424+03	.2335-03	-0000-
0000	121	263	-60.7	.1417+03	.2324+03	-6666-
04 71 60	120	264	-60.0	.1410+03	+2315+03	. 99 99
04 72 00	117	200	-61.1	1404+03	.2306+03	-6666-
G+ 73 G0	118	264	-616	7 +0	.2297+03	-0466-
00 \$7 \$0	117	265	-61.5	1390+03	.2288+03	-1000-
04 2500	116	266	-61.7		.2279+03	-9999
00 92	911	267	-61.9	9	.2270+01	-66.50
04 77 00	116	268	-62.1	41170+03	.2261+03	6666
04 78 00	1 00 1 04 1 04	267	-62.3	NO+N > 1 *	52	-6666-
00 64 90	121	265	-62.8	6+03	.2243+03	-9999
0008 40	120	266	-62.1	.1350+03	.2234+03	-6666-
04 61 00	119	267	-62.1		•2223+B3	-6666-
04 62 60	118	268	-62.7	.1336+03	21.	-6666-
04 83 00		270	-62.8	.1330+03	. 2202+03	-6660-
00 40 40	115	268	-62.8	.1323+03	.2192+03	-6666-
04 85 00		267	-62.0	.1317.03	.2181+03	***************************************
00 90 00	113	268	-62.8	.1310+03	.2170.03	.0000
04 67 00	113	268	-62.8		.2160.03	-4000
00 69 40	115	267	-62.9	.1298-03	RJ.	-6666-
00 68 47	115	266	-62.9	.1291+03	1	-0000
0006 00	114	265	-62.9	.1285+03	.2129+03	•60-60-
00 14 00	114	266	-62.9	.1279.03	.2114.03	****
04 92 00	7	265	-62.9	N	.2108+03	
04 93 00	-	264	-62.9	.1266+03	.2098+03	******
00 86 60	113	265	-62.9	0	.2088+03	-6666-
200	112	265	-62.9	. 1254.03	.2070.03	-1444-
00 96 10	1	26₩	-63.0	.1248+03	.2068+03	-000-
97	777	263	-63.0	. 1241+03	.2058+03	.0000-
00 86 10	112	263	-63.0	.1235+03		-4000-
03 66 40	112	262	-63.0	.1229+03	.2038+03	-6666-

17

	11. 11. 11. 11. 11. 11. 11. 11. 11. 11.	(DEG) 260 259 260 261 261 261	10EG C)	(MILLIBARS) -1223+03 -1217+03	(6RAM/N3) .2028+03 .2018+03 .1998+03	-9999- -9999-
	111 112 113 114 115 115 115 115 115 115 115 115 115	260 259 260 261 261 261	-63.0	.1223+03 .1217+03 .1211+03	.2028+03 .2018+03 .2008+03	.0000-
		259 260 261 261 261	-63.0	.1217.03	.2018+03 .2008+03 .1998+03	-6666-
05 02 00 05 02 00 05 03 00 05 04 00 05 05 00 05 05 00 05 10 00 05 12 00 05 13 00 05 13 00		260 261 261 261		1211+03	.1998+03	
05 02 00 05 03 00 05 05 00 05 05 00 05 07 00 05 10 00 05 12 00 05 13 00 05 13 00	100000000000000000000000000000000000000	261 261 261 261	C . 7 4 8		1998+03	-6666-
0503 00 0504 00 0505 00 0505 00 0506 00 0506 00 0510 00 0513 00 0513 00		261 261 261		1205+01		-6666-
05 04 00 05 05 00 05 06 00 05 07 00 05 10 00 05 11 00 05 13 00 05 13 00	112	261 261		10001	10404	-9999-
05 05 00 05 06 00 05 07 00 05 08 00 05 10 00 05 11 00 05 13 00 05 13 00	112	192			1979+03	-6666-
05 06 00 05 07 00 05 08 00 05 10 00 05 12 00 05 13 00 05 13 00	1111				1069-03	-6666-
05 07 00 05 09 00 05 10 00 05 13 00 05 13 00 05 13 00	100	263	1000	9 6	10401	-9999.
050800 051000 051100 051100 051200 051300	100	263	1 • 5 9 -	1174.03	1950+3	-6666-
65 C9 00 05 10 00 05 11 C0 05 12 G0 05 15 00	110 107 103 101 100 100 102	764	7.00	- 10	1041401	6666
051000 051100 051200 051300 0514 00	107 103 101 100 100 101	. 592	9		1041101	0
0511C0 051200 051300 0514 00	103 101 100 101 101	264	-03.0	50+1911	10,10,11	.0000
051200 051300 0514 0Q	101 100 101 102	266	-63.1	50+6511	50.27610	9990
051300	100	267	-63.2	1153+03	191300	9000
051460	101	267	-63.2	1147+03	50+1061	0000
	102	260	-63.3	.1142+03	5 D. CA 91 •	0000
05 15 00	***	270	-63.3	.1136+03	\$ D4884 \$	- 4444
	101	271	-63.3	.1130+03	.1877-03	****
20170	960	270	-63.4	.1125+03	.1868+03	•
	100	270	-63.4	.1119.03	.1859+03	6666-
	740	269	-63.5	1114+03	.1851+03	-6666-
		25.0	-63.5	.1108+03	.1842+03	-6666-
2000	940	265	-63.6	.1103.03	.1834+03	
		265	-63.7	.1096+03	.1825+03	0000
200000	180	265	-63.8	.1092-03	.1817+03	****
05.20	082	261	-63.9	1047+03	. 18 09+0 3	_
2000	083	259	-63.9		.1801+03	• 666-
26.26.00		257	-64.0	. 1076+03	.1793.03	-0000
06.37.00	***	255	-64.1	.1071+03	.1785+03	• 64 66-
20.2.50		253	-64.2	.1065+03	.1777+03	•6666
000000	0.85	255	-64.3	.1060+03	.1769+03	
20.4750	0.87	253	1-64.4	. 1055 +03	.1761.03	
00000	980	755	-64.8	.1050+03	.1752,03	6
001150	) (1	253	-64.4	.1045+03	.1743+03	n ii
22.70	080	254	-64.3	.1039+03	5D+96 4E	6
	060	254	-64. S	.1034.03	. 1725+D3	. 4
05 35 00	092	255	1.49-	.1029+03	1717403	
00 3% 00	093	255	-64.3	. 102 4 +03	1708+03	
051700	095	256	.64.3	. 1019+03	50.00/1	
	•60	258	-64.2	1014-03	50+1491•	
05.19.00	260	260	-64.2	. 1009 +63	20429T+	
000853	0.80	262	-64.2	1004-03	50+147	
004400	• 80	265	-64.2	. 999 1 +02	100010	
02.42.00	180	265	-64.3	20+2+66	.1659+03	- 4444
	710	266	-64.3	•	10.00.01	1
00 44 00	073	268	-64.3	•	1042403	
15	010	269	-64.3	.9795+72	50+05 9T •	
24.5	290	569	-94.4	.9747.02	50.4291.	
	990	269	-64.4	•	2	
	063	270		.9651+02		
•	040	271	5.49-	.9403-02	.1603+03	• • • • • • • • • • • • • • • • • • • •

TABLE 4. (Continued)

(FT / SEC   (OE 6)	DOICAL DAIA LAFE	n coffin	WIND DIRECTION	TEMPERATURE	PRESSURE		
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,		•	_	10E6 CJ	(MILLIBARS)	CONTRACTOR OF THE PROPERTY OF	
Color	;		26.7	-64.5	.9556+02	.1595-03	
10   10   10   10   10   10   10   10	DD		776	-64-6	.9509+02	.1589+03	- 4444
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	5100	059	997		9461+02	0	-0000-
10   10   10   10   10   10   10   10	00	055	207				****
0.00	00	950	264	0.00	70. FTF6.	F C 4 6 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	-0000-
10   10   10   10   10   10   10   10		250	263	-65.1	20.9964		
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,		250	263	-65.2	.9321+02	70	
Color			242	-65.3	.9275+02		• • • • • • • • • • • • • • • • • • • •
Color	20095		2 4 6		.9229+02	.1548+03	
10   10   10   10   10   10   10   10	99	•	107	4.54-	.9183+02	.1541+03	- 6666
10   10   10   10   10   10   10   10	00	053	107	46.4	.0117.02	.1535+03	-6666-
10	00	053	592	0.00	6046000	1528+03	-6666-
10	00	053	263	A-60-	20.2404	F C 4 C 7 4 F	-0000-
10		043	259	-66.8	70.4.08.	Э,	
10	,	110	258	-67.9	.8225+02	11396+03	
10   10   10   10   10   10   10   10	30		257	-66.7	. 782 3 + 02	.1320+03	
10		•	136	7-63-	. 744 3+02	. 12 38+03	•
Color	00	250	163	- 44-	7085+02	.1161+03	-6666-
10	06 10 00	0.12	522		4788403	11115+03	-0000-
10.5   2.5	20 00	030	254	6.70_		1052+01	-9999
10   10   10   10   10   10   10   10		0.28	256	-909-	70+ 17+0		
Color		225	258	-59.7	20.0219	30.80 AA	
10	200	22	787	-60.5	.5830+02	20+8256	
10	90		25.5	-60.1	. 5555+62	20-1906	- 66.66-
O	000	410	636		4202.02	. 86 57 + 0.2	-000-
100	000	*	9+2		204 5 40 8	A187+D2	-0000-
006         324         *583.04         *1556.02         *1556.	000	110	243	0.80	30.2500	17 42482	-66.6
100		900	546	-56.9	70. 90.84.		
100		100			2	40+0Cm) •	
Out		100		-56.6	2	2012011	
100	200		035	-57.2	•	-	
100			011	-57.1	-	.6421+02	*****
106		200		-27.0	•	.6127-02	***
100	00	010	50		1400+02	.5777+02	-0000
122   122	2000	110	90.	0 4	2042 442	.5478+02	76666-
100	00	600	122	7.50-		K205+02	-0000
193		100	6*1	-53.3	70+5875	****	******
007         205         -53.0         -53.4         -53		900	179	-52.3	3135+04	70.51.61	1
Color		001	193	-53.0	299 1 +02	20+557P.	
Color		200	205	-53.7	.2854+02	70+16-64	
000 255 002 2479 002 39 39 002 2479 002 255 003 2479 002 255 003 255 0		100	22.1	-53.6	.2723.02	20-1266	*****
010			201	-53.6	.2598+02	20+2214	
011 259 -51.9 .2365.02 .357.02 .357.02 .39.756.02 .99.99 .236.02 .39.756.02 .99.99 .236.702 .39.15.02 .99.99 .236.702 .39.15.02 .99.99 .236.702 .39.15.02 .99.99 .236.702 .39.15.02 .99.99 .29.20 .39.15.02 .99.99 .29.20 .39.15.02 .29.29 .29.2	200		386	975-	2479+02	. 39 39 402	
011 258 -53.3 .2257-02 .3516-02 .9516-0	000	5 3		0.15-	. 2365+02	.3758+02	
019 260 -53.5 .21.3.02 .32.56.02 -50.00 .32.56.02 -50.00 .30.00 .	000	110	(3)		2257+02	. 35 76+02	:
10   10   10   10   10   10   10   10	900	**	D C7		2153+02	.3415+02	\$
035 260 -53.0 .1960.02 .2953.0	030	410	097		205 0 +02	. 32 58 • 62	\$
030 260 -520 000 000 000 000 000 000 000 000 000	000	025	097	6.76	104040	.3102+02	
035 260 -52.3 .1779.02 .2667.02 -9099 -9099 -52.2 .1661.02 .2667.02 -9099 -9099 -52.2 .1508.02 .2590.02 -9099 -9099 -52.3 .1508.02 .2590.0	000	030	092	0.55		.2053+02	\$
040	100	035	260	4 · 2 C -	-	280640	\$
045 259 -52.2 .1608-02 .2535-02 -99 -99 -99 -99 -99 -99 -99 -99 -99 -9	000	0	260	-526.3	40.14.1	25.44.	-
050	000	900	259	-25.2	20+1691		
-52.0 .1959+02 .2790+02 .2790+02 .2990+			250	-52.2	<b>208</b>	20 55 57 ·	
00 259 -52-0 1454-02 -2290-02			259	-52.1	.1529.02	20+60 %2*	
. 20-20-1 1-23- 1-23- 1-33- 1-33- 1-33- 1-33- 1-33- 1-33- 1-33- 1-33- 1-33- 1-33- 1-33- 1-33- 1-33- 1-33- 1-33-	90	653			1454+02	20.04.22	-0000-
	500	000	167			.2178+02	-0440-

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TABLE 4. (Continued)

ALTITUDE	WIND SPEED	WIND DIRECTION	TEMPERATURE	PRESSURE	DENSITY	DEW POINT
(F1)	(FT/SEC)	(066)	(DEG C)	(MILLIBARS)	(68 AM/H 3)	(DEG C)
00 60 00	672	258	-52.2	.1314+02	.2017+02	:
09 70 00	070	250	-52.1	1249+02	2040704	
000860	****	258	4.55-			
09 90 00	040	25.8	-5.2 R	1120.02		
100000		26.7	1001	10.40404		
101000	082	260	-82.2	107.0407	162402	
102060	. 160	256		10+0140		
10 30 00	106	261				
109000	113	265	-51-7		20+01 <b>-</b> 1	
105000	116	261	-51.5	. 854 2+01	1343+02	-0000
100000	110	264	-50.2	3	1275+02	
10 70 00	01	259	-18.0	9	.1214-02	-6666-
10 00 00	119	259	-47.6	.7457+01	.1152+02	-1111
10 90 00	233	266	-46.3	10+1117.	.1093-02	-1999.
110000	135	26.0	-45.0	.6800+01	.1038+02	-0000-
11 1000	121	264	-43.7	.6492+01	.9856+03	-9999.
11 20 00	130	264	-12.4	.6203+01	.9364+01	-6666-
11 30 00	0*1	264	-41.1	-	.0913+01	-9999
11 40 00	9+1	260	-39.6	.5683+01	.8485+01	-6666-
115000	150	264	-38.5	5448+01	.6089+01	-6666-
116000	162	264	-37.2	.5213+01	1697-01	-0000-
11 70 00	. 157	265	-35.9	10-986	.7322-01	15
11 00 00	. 165	265	-34.6	.4774+01	.6972-01	-9199
119000	172	264	-33.3	.4560+01	.6651+01	-64.66-
120000	162	266	-32.0	1392+01	.63 84 + 01	-1111
121000	170	266	0.101	.4208+01	.6075+01	-1100.
DODZZI	185	7.92	-31.7	.4026+01	. 50 10+01	•
000521		27.1	# *** *** *** *** *** *** *** *** *** *	10+2+01	. 55 6 9 • 0 1	-0000-
0004.21	- 741		-31.0	3706+01	.5340+01	• 6666
2005	5 <b>6 6</b>	697	M · IN-	. 3550+01	10-1115-	-6666-
200464		407		10+000	10.9684	• • • • • • • • • • • • • • • • • • • •
		7 6	0.16	10.4076	10+96-94·	-0000-
20000	***	953	4.000	• 312 9 + 01		• 44 46-
130000			4:07	10.1000	10+2154	
131000	224	257		2740+01		
132000	222	256	M 1000	2644-01	איי	-000-
133000	526	253	-30.1	.2532+01	.3629+01	-1111
119000	201	252	-30.0	.2427+01	.3477-01	-9999-
135000	2:0	452	-29.0	.2326+01	. 3319+01	-9999.
136000	298	254	-28.0	10-6222-	.3167+01	-0000
	612	254	-27.0	.2140+01	2	***
13.60.00	142	253	-26.0		•	-6066-
000651	238	# S2 4	-25.0	*	.2764.01	-4004-
0000	234	757	-24.0	Į.	2	-000-
9907	622 622	82.0	-23.0	16.	N	
	97	236	0.22-	10	2	-6666-
	877	253	-20.6	- 2- 4-9-7 ·	9	-
	253	252	7.01-	9		-1000
37.5	7 7 7	233	-11.1	11542+01	10-2017	-4444.

METEOGOLOGICAL DATA TAPE

TABLE 4. (Continued)

ALTITUDE	=	WIND DIRECTION	TEMP ERATURE	PRESSURE	DENSITY	DEW POINT
	SEC	(DEG)	(DEG C)	(MILLIBARS)	(68 AM/M 3)	(DEG C)
,	231	253	-16.2	.1481-01	.2008-01	-6666-
	228	251	-14.8	.1423+09	10+6161*	-0000-
	238	247	-13.3	1370+01	.1837+01	-6666-
	226	246	0.11.	1118-01	1757+01	0000
	230	201		1244-01	10.00.41.	0000
10.01	282	200		1217+01	10.5041	-6686-
	287	280		1172+01	1547+01	-6666-
1000	080	0.50	6.01		10+00-11	-0000-
	265	250		1048-01	10-10-10-1	-6666-
	253	240	5-0-	1043401	1379+01	-8006-
6000	268	200	4	1003+01	11326+01	66.66-
	255	200		00+1146	1275+01	
	1 4 6	200	0	00-870-	1226111	-6666-
1	271	2 4 6	-10.0			
	1.2	0 4 7	Э С			
3300	673	943	э.	) (	10.17.17	
	9/7	957	-	000 1000	10.4401.	• 6666
	283	245	-	. 1937-00	10-2501	**************************************
	290	244	-12.3	.7622.00	.1018-01	-6666-
	292	244	-12.9	.7328.00	00+6086.	-6666-
65000	288	245	-13.5	. 705 3 +00	.9462+00	-6466-
	243	245		6787+00	. 1 25 100	-9999.
0000	275	266		4578-00	A7 94+00	-0000-
9952	256	26.7		427.4.00	00.47.50	0000-
	176	24.7	, 4	A012+00	00.00.00	-000
70000	260		•	00+1015	7858+00	-0666-
7 10 00	263	247		5571+00	7552+00	-6666-
7 20 00	271	247	-17.5	5454.00	.7295.00	-9999.
7 30 00	280	247	-20.3	. 5144+00	70.87+00	-9999.
74000		246	-22.2	00.6164	. 66 55 + 00	-9999.
75000		249	-22.2	.4742+00	.6582+00	-9999
7 65 00	308	250	-20.2	00+828 m	.6272+00	-9999
1	90S	251	1012	00+3214	00+9009	-6666
	908	152	7 ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) (	00+1064		-9966-
	107	252	-21.2	4017+00	. 44 8 1+00	-69.65-
0.000	302	252	-25-1	3476+00		9999
	300	252	-28.9	. 1719+00	5304.00	-9999.
2000	298	252	-31.2	3566+00	.5133+00	-9999.
200	300	252	- 12.2	00+014	. 4942+03	40.66-
	30F	25.2	12.2	1278400	00+0744	*****
	8.10	26.2	-11.2		44.21020	
	***	262	6.86		0048444	
9000						
	# P	25.5		00+1466		
36		7 20				0000
	7 6	24.5	6 46	00.099.		
3	200	200		1		
0	725	957	2.07-	00-8-20	20+10+6	
	on n	282	7-82-	20.4.400	00+0455	
		259	-28.2	.2253+00	.3204+00	-6446-
	347	260	-27.5	.2162-00	.3066+00	-6666-

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TABLE 4. (Continued)

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TABLE 4. (Continued)

• (	2	WIND DIRECTION	TEMPERATURE	PRESSURE	DENSITY	0
(FT)	(FT/SEC)	(0EC)	(DEG C)	ø	I	
24 60 00	175	261	-78.2	.2280-01	.4073-01	-6666-
200	175	260	-80.0		.3896-01	-6666-
24 80 00	172	260	-81.2		.3720-01	-6666-
24 90 00	1.70	260	-82.6	046	10-7485	
25 00 00	170	259	-83.2		•	_
25 10 00	168	259	-83.2	75	◐	•
25 20 00	167	258	-83.2	. 1660-01	#	-6666-
25 30 00	160	257	~	0	.2915-01	-6666-
25,40 CG	152	257	N	525	7	-0666-
25 50 00	145	256	_	458	<b>ار</b> ا	-6666-
25 60 00	138	256		-		6
25 70 00	130	256	-80.2	337		6
25 90 00	123	255	-79.7	.1281-01	-	-6666-
25 90 00	116	452	-79.1	. 1226-01	0	•
26 00 00	108	.254	-78.5	.1175-01	53	-6666-
26 10 00	101	253	-77.9	.1125-01	62	-6666-
26 20 00	*60	252	-77-3	.1077-01	. 19 75-01	-6666-
26 30 00	086	251	-76.8	.1032-01	.1691-01	6666-
26 40 00	079	250	-76.2	9879-02	. 18 11-01	6666-
26 50 00	210	248	-75.6	.9461-02	.1735-01	6666-
26 60 00	065	297	-75.0	. 906 1 -02	-	6666-
26 70 00	050	544	*	.8677-02	.1591-01	6666-
26 80 00	051	241	-73.9	.8310-02	.1524-01	6666-
27 10 00	6 <b>₹</b> 0	245	-78.4	.7130-02	.1250-01	6666-
274000	940	249	-75.0	0	. 10-001	6646-
277000	***	252	M	0	.9250-02	-6666-
28 CO DO	0.38	256	-76.1	0	- 79 50-02	6666-
28 30 00	027	526	-76.7	0	.6840-02	6666-
00.0982	016	265	•	0	80-0	6666-
000687	900	295	-77.9	830	.5060-02	6666-
29 20 00	800	034	-78.5	0	20-0	6666-
000567	018	054	-79.1	90	20-0	-66.66-
20 00 00	970	289	-78.5	0	20-0	0
	-	2/2 2/2	∴.	5	0-02	666
	177	212	2.01	20-0 \$210	0-081	D (
		270		20-0901	100	6666 6666
33 30 00	2.50	260	9.00		20-07-01-	A 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
316000		26.0	0.04	Э С	30-05-51	. 0
319000	152	240	•'	3 6		- AB AB
322000	751	0 40			۰.	Ň
32 50 00		249				900
32 80 00	710	269	-61-1		8 80.0	Ò
33 10 00	1,0	269	-	10	0-000	
334000	062	268	m	760	~	
33 70 00	047	267	6.64-	.2390-03	90-0	2000-
34 00 00	025	262			20-05	0000
4 30 0	400	125	N	1790-03	0-06	6
	027	960	-37.5	0	2 00	6666-
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TABLE 4. (Concluded)

ALIMOR	OLIVE OF THE	WIND DIRECTION	TEMPERATURE	PRESSURE	DENSITY	DEW POINT
	(71/550)	10561	(DEG C)	(MILLIBARS)	CON AM/H 31	1056 (1)
000766	033	nat	-24.5	.1210-03	.1610-03	-6666-
35 50 00	037	102	-16.6	.1060-03	.1380-03	-6666-
35.80 60	X 6 0	104	-12.4	.9300-04	F G-09 11	-6000-
36 10 00	043	660	-6.0	.0-170-04	1010-03	0666-
364000	045	101	- M	.7360-04	#0-0878°	0000
36 70 00	047	105	12.6	, 666 G - G4	7640-04	-6666-
37 00 00	640	109	23.8	*0.000	. 66 50-04	6600-
37 30 00	020	113			47.00-04	0000-
376000	051	61	****		***************************************	0000-
37 90 CO	045	109	50.7	80-0 F#*		0000
38 20 00	240	112	62.0	#0-050#1	#U-U-05"	0000
38 50 00	042	91111		4740-04	40-04 AV	0000
38 80 00		120	. 4	40 C 94 F		0000
101010	0.00	200	0 0	10-06+6+	*D-0016*	
		170	7 6	#0-00Zc •	10-0/17	****
3	932	671	D-111	PO-0162.	*0-08 *Z*	***
29 70 00	8 60	134	123.9	.2770-04	.2230-04	-6666-
40000	038	139	137.1	*2590-0#	•2020 <del>-</del> 04	-6666-
-0 66 6-	*6666-	-6686-	-6666-	î	6660-	-9999
-6666-	-6666-	*0000-	0000	00000	000	00001
-9000-	00001	-0000	0000	00001	0000	
0000-			4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	-0.000	****	****
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-6666-	*6666-	*66661	-0666-	-6666-	6066-	-0000-
-6666-	-6666-	-9999-	- 6666 -	-0000-	- 6666-	-6666-
-0000-	-6666-	*6666-	-9000-	.0000	- 0000-	-0000-
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****	6666	• 6636-	6666-	-6666-	• 6666 •	-6666-
•	6666-	-6666-	* 6666	-0000-	• 6666-	-6666-
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	-6666-	-666C-	-0000-	-6666-	-6666-	-6466-
-6666-	-0666-	6666-	-6666-	-6666-	- 9999	-0000
-6666-	-6666-	-6666-	- 6666-	-0000-	6666-	-0000-
-6666-	-6666-	-6666-	- 6666-	-0660-	- 0000	-0000-
-6666-	•66661	-6666-	. 9999 -	6666-	6666-	0000-
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-0 66 6-	-6666-	46666-	60001	00001	00001	0000-
-9499-	-6666-	-6666-	0000	00001	0000	0000-
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	66661	-6666-	• 6666-	°6666-	• 6666 <b>-</b>	-6666-

STS-2 FINAL SRB DESCENT METEOROLOGICAL DATA TAPE TABLE 5.

HETEOROLOGICAL DA	1	1				
111100	0	WIND DIRECTION	TEMPERATURE	PRESSURE	DENSITY	DEG POIN
(FT)	(FT/SEC)	(066)	(DEG C)	(MILLIBARS)	(GRAM/M3)	(0E6 C)
090000	480	325	21.0	.1012+04	.1189+04	17.8
00100	028	900	20.4	.9780+03	.1152+04	16.9
002000	025	352	0	-9443+03	7	16.4
003000	026	1 S S S S S S S S S S S S S S S S S S S	•	114+	88	16.2
000 000	026			794+	-	4.01
000 500	030	333	-	4 8	29	3
000 900	037			180+	8.7	-13.2
8	035	325	11.7	888	.9640+03	-18.1
_	042	322		.7605+03	•	
000600	020	323	8.1	.7330+03	.9074+03	-22.0
010000	0.50	321	8.9	. 7064+03	.8786+03	
~	050	312	6*5	.6806+03	.8493+03	-24.4
$\sim$	054	309		557	221	-24.6
013000	059	312	2.1	.6316+03	.7973+03	1.4.7
C14000	061	310	80.	*	.7731+03	-27.6
015000	062	309	0.1	0	06	-29.9
016000	190	308	-2.6	1	14	=31.6
017000	990	308		*	284	- 52 B
CIBODO	190	308			824+	9 4
000610	940	202	0		•	
02000	062	300		200	7	1 30.1
02100	140	101		444	2 2 2	F C 3 t
022000	040	201			o lo	
02100	2000	100	9	777	50175001 5047403	0.24
000 920	5 C C	* O. P.	s c	9 9	. 444	'n
025.00	0 0	, ,	•	0 4 6 6 0		
00033	, so C	900	7 6 0	4777404	7007	- 0 t 1
027,000	960	, O. F	27.7	9 0	100	9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9
2:5	97.0		- 0	• •		
2	3 at	276	; =	405	707	
2 5	000	280	• 5	100		n 4
Š	000	2000		9 0		
Š	-	111	0 0			0.001
033000		800		9 -		
034,000	120	40.8	••		10	ď
035000	124	305	. 2	2+0	856+0	. 0
036000	114	294	143.5	0	701+0	-61.2
037000	103	281	•	•	559+	-61.7
038000	098	271	9.94-	.2228+03	.3429+03	-63.2
039000	160	269		.2128+03	290+0	0.49-
000000	160	271		32+0	2+0	5.19-
000140	660	271	6.64-	÷ 7 7	028+0	-65.4
042000	100	270	:	52	0	-66.5
043000	660	564	~		190+0	-67.5
•	00 <b>1</b>	260	-	٠	0	-67.9
045000	103	255	ιά: • • • • • • • • • • • • • • • • • • •	60	552+0	-68.1
900	103	252		35+	0+075	-58.5
4700	860	256	0 · d.	+ + 9	336+	-64.3
BO 1		265	S • S • S	96	235+	-10.5
000617	560	•	-56.1	.1331+03	.2137+03	-71.0

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METEOPOLOGICAL DA	DATA TAPE	MOTO OTO	TEMPEDATIOF	POFCCHAF	DENSITY	NIO4 MBG
16.11.006	ייייייייייייייייייייייייייייייייייייי	1 1 1 1 1 1 1		: =	(GRAM/H3)	(D 5 7 C)
_ ;	י / אני מיי	105.01	1 10		2041402	7
020000	0.60	597	n ı		5 6	7 12 1
2	083	258	-51.3	-	֓֞֜֜֜֜֜֜֜֜֜֜֜֜֜֜֓֓֓֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜	0.17
025000	075	250	-57.9		.1867+03	0.21.
053000	190	242	-58.0	.1099+03	<b>÷</b>	1.27-
00	060	235	-58.1	.1948+03	.1697.03	12
5500	055	231	-58.9	20+#856°	.1623+03	
026000	051	232	-60.0	.9513+02	.1555+03	•6666-
5700	045	241	-60.6	.9062+02	.1485+03	.6666-
20	039	255	-59.8	.8632+02	.1409+03	9
02000	980	264	-59.3	.8225+02	.1340+03	-6666-
000000	0.35	271	-58.7	837+0	.1273+03	-6666-
000000	250	272	- 10	20+0242	.1206+03	-6666-
2	0 C	263	ூ	.7121+02	.1146+03	-6666-
202200	8 20 0	23.5	ı	20+05/9	.1087+03	-6666-
	2.0	316	0 1 3 1	6476+02	.1034+03	-6666-
9 4	7 4 6	205	1	.6177+02	9824+02	*6646-
0 4	213	200		5893+02	~	-0000-
o r	2 6 6	97.°	1.02	5623+02	8 7	-6666-
2 6	<b>N 9 0 0</b>	617		5.5.46.7+0.2	8458+02	.6666-
00000	800	96.3		*D-1066	-80324D3	6666-
000690	000	<b>*</b> 97	1961	20 271C.	7672+02	0
000070	900	997	7.16.	*O. P. C.	10.3.01	0000
071000	800	279	) • 6 h =	20+/00+	70.0/2/	- KKKK
012000	011	289	3.03	27+15ts.	70+8049*	****
000820	012	286	-	425/+32	70+9959*	****
000 110	012	282	-47.2	2f + 190 h •	77	*****
015000	012	282	-46.7	3886+02	2948462	****
016 000	0 14	287	146.1	. 3713+02	20+1495	• 6666
00110	017	295	-46.2	20+8+05	70+9465	* A A A A
078000	018	568	-46.3	3390+02	.5206+02	. 4444-
8	017	294	3.03	.3240+02	20+926+02	*****
8	016	288	r. # 81	20+1605	20+52/6	****
C81 000	015	283	-43.6	.2960+02	20+26##*	6666-
8	<b>51</b> 0	273	-42.5	.2031+02	27	-6666-
083000	015	272	2	707+0		• 6666-
000 400	026	288	-41.8	.2539+02	.3899+02	6666-
85	240	297	-41.6	.2474+02	.3725+02	6666-
C86 000	190	298	-41.2	.2 .69 + 62	.3558+02	6666-
087 000	082	298	٠	.2566+02	.3397+02	6666-
C88 000	680	296	•	.2367+02	.3245+02	*****
8	088	293	-40.7	.2273+02	.3107+02	6666-
000060	083	286	-40.5	1784.02	.2971-02	6666-
5	080	277	-40.2	.1698+32	.2838+02	6666-
8	010	268	1.08-	.1816+02		-6666-
000 £60	010	262	-38.0		518	.6666-
000 +60	079	261	-36.6	.1663+02	.2449+02	6666-
002500	010	263	-36.4	.1593+02	# # M	-6666-
000 960	080	269	-36.2	.1.25+02	.2242+02	-6666-
000160	082	274	-35.7	.10+02	.2142+02	-6666-
000860	280	276	-35.0	.1.,8+02	S	9
00	680	258	-35.U	.1326+02	.1940+02	-6666-

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TABLE 5. (Continued)

WIND SPEED (FT/SEC)	MIND DIRECTION (DEG)	-0	PPESSURE (MILLIBARS)		OEU POINT
087	267		.1258+02	•	-6666-
082	260	-34.6	-1194+02		-6666-
76	256	3	-1133+02	.1653+02	
907	197	2.4.5-	1075+02	95	
· ·	265	<b>.</b>		984	-6666-
91	197	יי	In+2/96*	70+90+11	*****
9 1	197	2 1	10.9/16.	•1 536 •UZ	*****
601	259	2		.1266+02	*6666-
611	259	- N N -	528+	200	0
133	266	-33.2	.7836+01	.1138+02	-6666-
135	268	*	.7434+01	1079+02	-0000-
121	264	-32.9	.7053+01	2	-6666-
130	564	-32.8	10+1699*	.9698-01	-6666-
140	264	-32.7	.6348+01	.9197+01	-6666-
146	.260	-32.6	m	2	-6666-
158	264	· ~	7	8758+01	-0000-
162	264	-	F452401	7841+01	D
157	26.5	, ,	127	10. F10.	. 0
16.5	25.5	2	10.0740	7052401	0000-
172	26.4	2 2	10:4:04	. 6.687+D1	-0000
182	25.6	: :	10.7.20.4	10000	0000
170	26.6	٠ ۲	**************************************	777	• •
195	26.7	9 j . 4 j e=	10.007		0000
001	27.1		10:0301	10.0100	0000-
197			10:3055	10 - C 20 - C - C - C - C - C - C - C - C - C -	0
	250	:=		1 2	0000-
179	269	-31.	10+m0+m•	10 + 80 + 8 + 10 11 11 11 11 11 11 11 11 11 11 11 11	6666-
175	263	-	• 3264+01	**************************************	-6666-
182	258	-30.9	.3129+01	10+6644	0666-
197	255	-30.7	.3001+01	.4312+01	-6666-
216	255	-30.6	.2878+01	.4134+01	-6666-
224	25.7	-30.4	.2760+01	.3961+01	-6666-
222	256	-30 • 3	.2644+01	.3792+01	-6666-
229	253	•	.2532+01	.3629+01	-6666-
241	252	-30.0	.2427+01	.3477+01	-0000-
544	254	-29.0	.2326+01	.3319+01	.6666-
248	254	-28.0	.2229+01	.3167+01	-6666-
546	254	-27.0	.2140+01	.3028+01	-6666-
244	25 3	-26.0	.2053+01	.2894+01	-0000-
238	254	-25.0	+696	.2764+01	-6666-
234	257	-24.0		.2540+01	-0000-
229	258	-23.0	12.	•	-6666-
236	256	-22.0	•	2910+01	-0000-
248	253	0	• 60	<u> </u>	-6666-
253	25.2		1604	199	-6666-
243	253	-	1542	٠	-8888-
231	253	116.2	1481	٠	-6666-
228	251	3	1423+	616	*6666-
238	7 4 7	-13.3	1370	837+	-6666-
			,		•

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TABLE 5. (Continued)

ALTS TUDE	WIND SPEED (FI/SEC)	WIND DIRECTION (DEG)	TEMPERATURE (DEG C)	PRESSURE IMILLIBARS)	GRAM/M3)	OEU POIN
	2 /0	247	-10.4	.1266.01	•619	O
	262	248	0.6-	217•	.1605+01	6666-
	287	6#2		.1172+01	.1547+01	6666-
	280	250	•	1129+01	06	Ф.
	265	250	#*6-	086	-	6666-
	253	546	5-6-	.1043+01	4	6666-
	248	546	9.6-	.1003-01	.1326+01	6666-
	255	248	-9.1	643	.1275+01	6666-
	265	248	0.6-	.9278+00	.1229+01	6666-
59000	271	246	-10.0	ž	.1183+01	6666-
00009	275	248	-10.6	.8597+00	. 1 14 1 + D1	6666-
61 000	278	546	-11.2	3	1046601	6666-
000	283	245	-11.7	.7937.00	.1058+01	6666-
	290	244	-12.3	.7622+00	.1018+01	6666-
94 000	292	544	~	28	809	6666-
65 000	208	245		.7053+00	9462+00	6666-
66 000	283	245	1	. 6787+no	9125+00	0000
000	275	246	•	.6528+00	.8796+00	6666-
000 89	256	247		76	476	6666-
00069	261	24.7		032	8176+00	6666-
20007	260	747		5797+00	00+8587	0000-
71000	263	24.7		5571+00	ď	0000
72000	271	24.7	-17.5	5354+00	1	5666
73000	280	247		5144+00	. 0	6666-
24 000	290	24.8	2	00+626#	• 6655 + 00	6666-
75 000	298	545	-22.2	. 4742+00	.6582+00	6666-
16 000	305	250	-20-2	5	.6272+00	6666-
77 000	309	251	4.64-	75	00+9009*	6666-
78000	309	251	-18.2	-4203+60-	.5742+00	6665
79 000	307	252	-21.2	.4037+00	.5581+00	6666-
80000	302	252	'n	.3876+00	.5444+00	6666-
91 000	300	252	-28.9	.3719+00	.5304+00	6666-
82000	298	252	-31.2	.3566+00	.5133+00	6666-
	300	25.2	-32.2	3419+00	.4942+00	6666-
84 000	305	252	-32.2	.3278.00	. 4 T38+00	6666-
85 000	310	252	-31.2	$\sim$	.4523+00	6666-
86 000	317	252	-28.7	.3014+00	.4295+00	6666-
000	352	253	-27.2	.2891+00	<b>3</b> 60	6666-
88 000	327	253	•	.2774+00	.3944+00	6666-
00069	331	254	Ф.	.2660+00	.3797+00	6666-
00004	# P P	255	-58.5	2+0	659	6666-
000	337	256	•	9		6666-
000	339	25.7	ø		.3340+00	6666-
93 000	## P	259	-28.2	₩.	.3204+00	6666-
000 to	247	260	-27.5	N	90	6666-
	351	292	-24.6	15+	.2908+00	6666-
96 000	356	264	-20.7		. 2749+00	6665
	359	256	-17.7	7.0	0 1 4 + 0	6666-
000	363	24.1	4,214	E042 40 F	4	93661
	, , ,		P		00	4444

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TABLE 5. (Continued)

ζ.	(0 9 30)	-6666-	-6666-	-6666-	-6666-	-0000-	-6666-	-6666-	-6666-	-6666-	-6666-	-6666-	• • • • • • • • • • • • • • • • • • • •	-0000	-0000-		-6666-	-6666-	-6666-	-6666-	-6666-	6666-	6666-	-6666-	-6666-	-6666-	-6666-	-6666-	****	-6666-	-6666-	-6666-	-9999	• • • • • • • • • • • • • • • • • • • •	0000	-0000-	-6666-	6666-	-6666-	-6666-	-6666-	-6666-	*6666-	6666	. 60000	. 4444
DENSTI	(GRAH/M3)	.2336+00	.2255+00	.2173+00	.2104+00	021	9 4 8	87	.1814+00	.1752+00	.1685+00		.1549+00	20+54	- 4	200	1244+00	195	.1151+00	.1104+00	.1062+00	.1026+00	10-1440	.9290-01	.8969-01	.8621-01		•	10-59/10		•6939-01	.5708-01	.6501-01	.6260-01 4 of 1-01	10-1000	10-8586	.5429-01	. \$239-01	.5027-01	9 4 6	652-0	10-11-01	10-424-01	10-8404	9 4 6	.3720-01
RESSURE	(MILLIBARS)	.1711+00	.1644+00	.1579+00	-	1456+00	9	~	•	~	.1187+00	.1138+00	.1092+00	? ?	000011	10-0554	8890-01	.8540-01	.8200-01	.7870-01	.7550-01	.7230-01	.6930-01	10-0819-	.6130-01	.5890-01	9	.5410-01	10-0/15*	10-04-4	.4510-01	.4310-01	.4120-01	.3930-01	10-06/5	10-00-6	3250-01	60	_	_	.2660-01	.2530-01	10-00-2	.2280-01	10-0472	.2050-01
Z Z Z	(DEG C)	-16.0	-19.2	-20.0	-	2	-23.2	-24.1	-25.6	-27.1	7.	-28.2	-27.6	7.12	0 4				-24.9	-24.9	-25.4		N 1	25.54 23.69	m	-35.2	-36.2	38		6 - 5 B = -	9	-49.3	2		n u c u			-	-69-	-71.8	:	•	5-11-	-78.2		-81.2
WIND DIRECTION	(DEG)	270	271	272	272	272	272	272	27.1	270	569	26.7	264	192	867	25.1	24.7	- PT - C	240	237	234	233	232	231	23.2	233	234	236	231	24.2	75.	24.7	545	251	567	25.5	25.8	259	259	260	260	260	261	261	097	260
WIND SPEED	(FT/SEC)	364	364	363	359	354	349	##M	339	332	325	319	310	* C C	167	288	285	2 C C C C C C C C C C C C C C C C C C C	282	282	280	280	278	27.5	270	592	260	253	246	223	228	221	216	2112	907	707	****		101	185	192		179	175	175	172
ALTI TUDE	(FT.)	200000	201000	202 000	203000	204 000	205 000	206 000	201 000	208 000	209000	210000	211000	212.000	212000	r v	12	217 000	219 000	219 000	220000	221 000	222 000	224 000	225 000	226 000	227 000	228 000	000 622	241 000	232 000	2 3 3 000	234 000	235000	236 900	237 000	200	240000	241000	242 000	243000	244 000	245 000	9		248 000

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TABLE 5. (Continued)

	MIND SPEED	WIND DIRECTION	TEMPERATURE	PRESSURE	OEMSI II	200
	(FT/SEC)		U	MILLIBAKSI	CKARAL TO	ומנים כי
	170	259	-83.2		.3374-01	. 4444
	168	259	-83.2	.1750-01	.3209-01	-6666-
	167	258	-83.2	.1660-01	.3044-01	-6666-
	160	25.7	-82.6	.1590-01	.2915-01	-6666-
	152	25.7	-82.0	.1522-01	.2791-01	-6666-
	345	256	-81.4	.1458-01	.2673-01	-6666-
	138	256	-80.8	.1396-01	.2560-01	-6666-
	130	256	-80.2	.1337-01	.2452-01	-6666-
	123	255	-19.1	.1281-01	.2348-01	-9999.
	116	254	-79.1	.1226-01	10-6422*	-6666-
	108	254	-78.5	.1175-01	.2153-01	-0000
	101	253	-77.9	.1125-01	.2062-01	-6666-
	160	252	-77.3	.1077-01	.1975-01	-6666-
		251	-76.8	.1032-01	.1891-01	-6666-
	640	250	-76.2	.9879-02	.1811-01	-6666-
	072	842	-75.6	.9461-02	11735-01	-6666-
	065	247	-75.0	.9061-02	10-1991	-6666-
	058	.244	-74.4	.8677-02	.1591-01	-6666-
	051	241	-73.9	.8310-02	.1524-01	-0666-
	040	245	7.5-	.7130-02	.1250-01	-6666-
1	9#0	249	-75.0	.6120-02	.1080-01	-6666-
	**0	252	-75.5	.5250-02	.9250-02	-6866-
	038	256	-76-1	. \$500-02	.1950-02	-0000-
	027	259	-16.1	.3660-02	.6840-02	-6666-
	016	265	-77.3	.3300-02	.5880-02	-6666-
	900	295	-77.9	.2830-02	.5060-02	-6666-
	900	034	-78.5	.2430-02	. 350-02	-6666-
	019	05.4	-79.1	.2060-02	.3750-02	-6666-
	020	289	-78.5	.1690-02	3020-02	-6666-
	<b>\$10</b>	275	~	.1450-02	2570-02	.6666-
	117	212	-76.2	.1240-02	.2180-02	*6666-
	150	271	-75.0	.1060-02	.1850-02	-6666-
	164	270	-73.8	.9050-03	.1570-02	-6666-
	159	269	-72.2	. 7770-03	1330-02	-6666-
	158	269	6.69-	.6690-03	.1130-02	-6666-
	152	569	-67.7	.5760-03	900	. 6666-
	137	569	-65.5	.4970-03		6666-
	114	569	-63.3	. 4280-03	.6920-03	-6666-
	017	569	-61.1	.3680-03	.5880-03	-6666-
	071	269	-57.4	.0-0315	ED-056#*	*6666-
	290	268	~	.2760-03	.4240-03	6666-
	0.47	267	0.01-	.2390-03	.3590-03	6566-
	025	262	-46.2		.3050-03	-6666-
	200	125	~		.2590-03	-6566-
	027	960	-		.2200-03	-0000-
!	030	860	-31.2	.1370-03	0-0	-6666-
	033	100	-24.9	.1210-03	0-0	- 6666-
	037	102	-18.6	.1060-03	.1380-03	-6666-
	T .0	104	-12.4	*0-D08 6*	.1160-03	-6666-

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TABLE 5. (Concluded)

ALT'S TUDE	WIND SPEED	WIND DIRECTION	TEMPERATURE	PRESSURE	DENSITY	_
1673		_	(DEG C)	(MILLIBARS)	(GRAM/M3)	(C 5 30)
364 700	4 2	101	3.3	.7380-04	.6780-04	-6666-
367.000	Z * 0	501	12.6	.6660-04	*D-D*91.	-6466-
20000		801	-	*0-0009*	*0-D599*	-6666-
173000	050	113	•	#0-00#S*	.5790-04	-6666-
376.000	051	119	7.00		.5040-04	-9999
379 000	S#0	109	50.7	*410-04	*4 # 30 - 0#	-6666-
382 000	2 00	112	62.0	*0-050**	.3920-04	-6566-
385 000	240	116	73.8	.3730-04	*3*80-0#	-6666-
388 000	0 4 3	120	85.9	.3450-04	.3100-04	-6666-
391 000	040	124	98.3	*3200-04	*2770-04	6666-
394000	039	129	111.0	.2970-04	.2480-04	-6666-
397 000	038	134	123.9	.2770-04	*2230-0#	-6666-
4.90 0.00	038	139	137.1	*2590-04	*5050-0#	-6666-
-6666-	-6666-	• 6666-	-6666-	-6666-	-6666-	-6666-
-8666-	-6666-	-6666-	-6666-	-6666-	-6666-	-6666-
-6666-	-9999-	-6666-	-6666-	.0700-	*6666-	6666-
-6666-	-6666-	-6666-	-9999.	-6666-	-6666-	-6666-
-6666-	-6666-	-6666-	-6666-	-6666-	-6666-	-6666-
-6666-	-6666-	-6666-	-0000-	-6666-	-6666-	-6666-
-6666-	*6666-	-6666-	-6666-	-6666-	* 6666-	-6666-
-6666-	-6666-	-6666-	-6666-	-6666-	-6666-	6666-
-6666-	-6666-	-6666-	-0000-	-6666-	•6666-	6666-
-6666-	-6666-	-6666-	-6666-	•6666-	.6666-	•6666-
-6666-	-6666-	-6666-	-6666-	-6666-	.0000-	. 6666-
-6666-	-6666-	•6666-	-6666-	. 6666-	-6666-	. 6666-
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STS-2 SRB DESCENT-IMPACT SURFACE SHIP OBSERVATIONS TABLE 6.

Site: USN Ship, Gen. H.S. Vandenberg				
Location: 30°N Latitude 78°W Longitude				
Date: November 12, 1981 Time: 1517Z				
Surface Observation:				
Air Temp. of Wet-Bulb of Dew Pt. of		Pressure (MSL) mb	Wind Dir.	Wind Sp. Kt.
68.8 65.5 . 64	10	1013.4	325°	20
Sky Observation:	Total Chy	E	\$	77:
Clouds	Cover	Opaque Sky		(miles)
7/10 Stratocumulus at 1,800 ft	7/10	7/10		7
Sea Observations:				
Sea Condition:	Wind Waves:	Swell C	Swell Conditions:	
Sea Slight - Code 5 6/10 Breaking waves	Freq. Ht. Sec. m.	Data N	Data Not Available	
4/10 Foam Surface Sea Water Temp = 83.5°F	9			

TABLE 7. SELECTED ATMOSPHERIC OBSERVATIONS FOR THE FLIGHT TESTS OF THE SPACE SHUTTLE VEHICLES

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		Count Down and Launch Comments Dir. of Meteorological (deg) Significance		
wind Below 60 000 ft		Dir. (deg)	350	286
		Speed (ft/sec)	8	158
		Alt.	44 300	36 300
		Dir. (deg)	125 120	345
		Speed Dir. (ft/sec) (deg)	11.8 15.2	27.0
Observ		Rel. Hum.	82	61
Surface Observations	Thermodynamic	Temp.	21	23
	Thermo	Press N/cm <sup>2</sup>	10.234 <sup>d</sup>	10.166 <sup>e</sup>
		Launch Pad	39A	39A
Vehicle Data		Time <sup>b</sup> (EST) Neares. La	0040	1010
		Launch Date	STS-1 4/12/81	11/12/81
		Seq. Vehicle No. No.	STS-1	STS-2
		Seq.	1	2

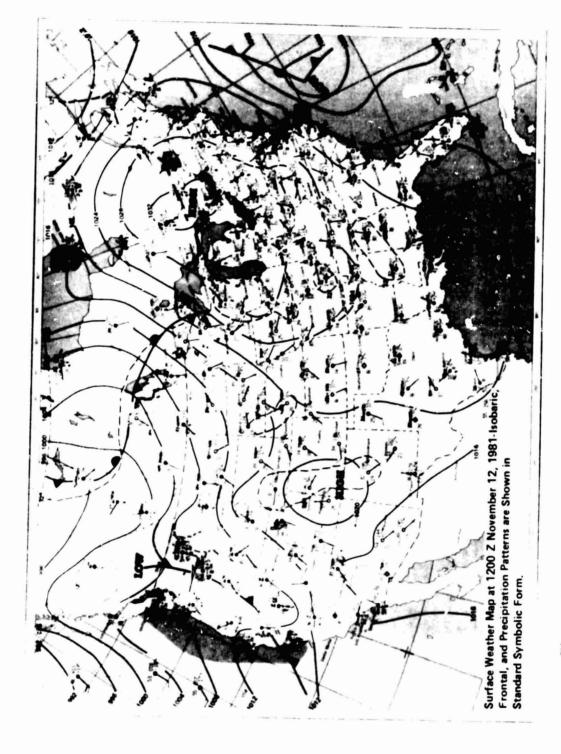
camera site No. 3. a. Pad 39A thermodynamic measurements taken at approximately 1.2 m (4 ft) above natural grade at

b. Eastern Standard Time unless otherwise noted.

I min average prior to T+0 of 60 ft PLP (listed first) and 275 ft FSS winds measured above natural grade. . :

d. Pressure measurement applicable to 14 ft above MSL.

Pressure measurement applicable to 21 ft above MSL.



Surface weather map 3 hr, 10 min prior to launch of STS-2. Figure 1.

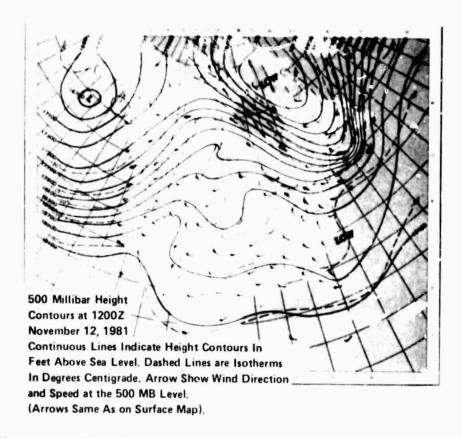


Figure 2. 500 mb map 3 hr, 10 min prior to launch of STS-2.

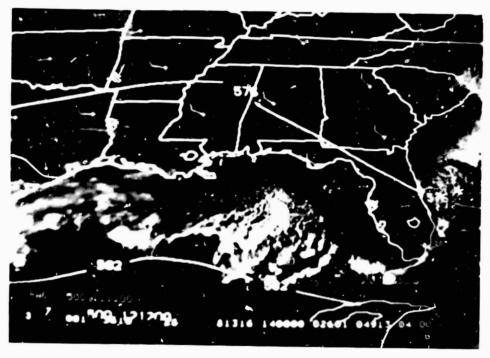


Figure 3. GOES SMS-II visible imagery of cloud cover 1 hr, 10 min prior to launch of STS-2 (1400Z, 12 November 1981).

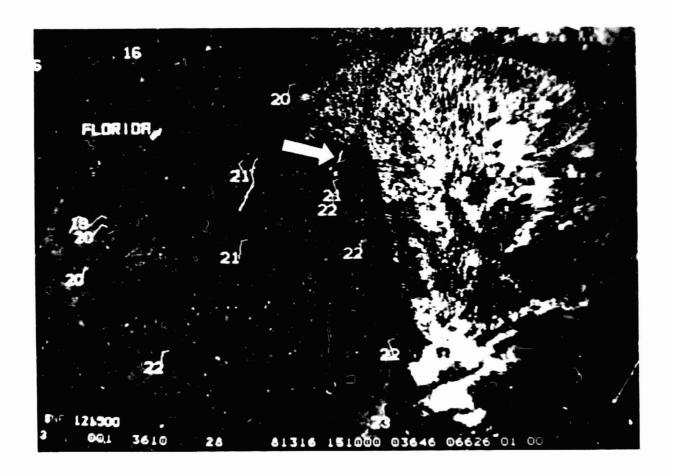


Figure 4. Enlarged view of GOES SMS-II visible imagery of cloud cover with exhaust trail visible (indicated by arrow) during launch of STS-2 (1510Z, 12 November 1981). Figure includes 1500Z surface observations of temperature and winds for surrounding Florida sites.

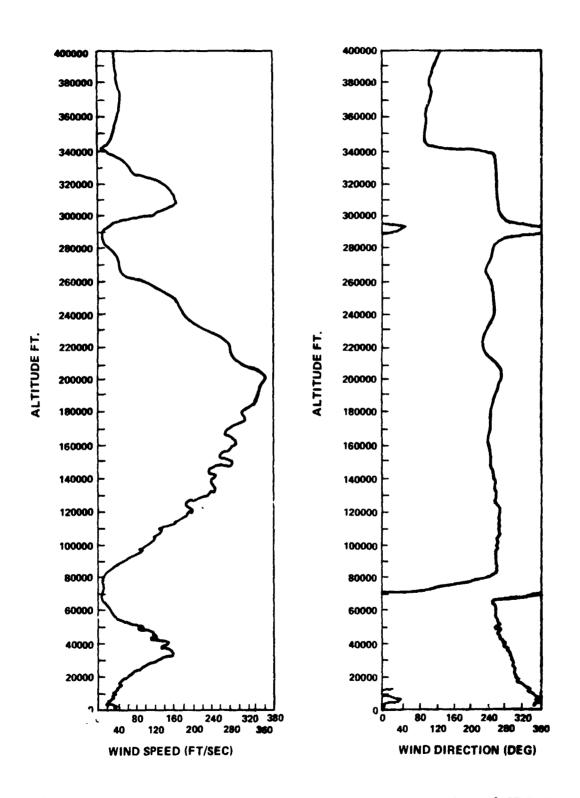
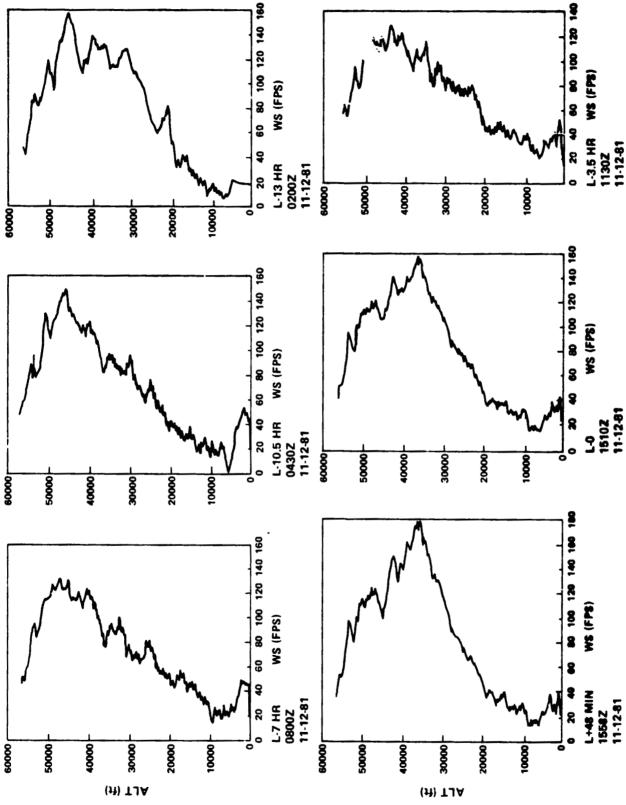


Figure 5. Scalar wind speed and direction at launch time of STS-2.



STS-2 prelaunch/launch Jimsphere-measured and estimated wind speeds (FPS). Figure 6.

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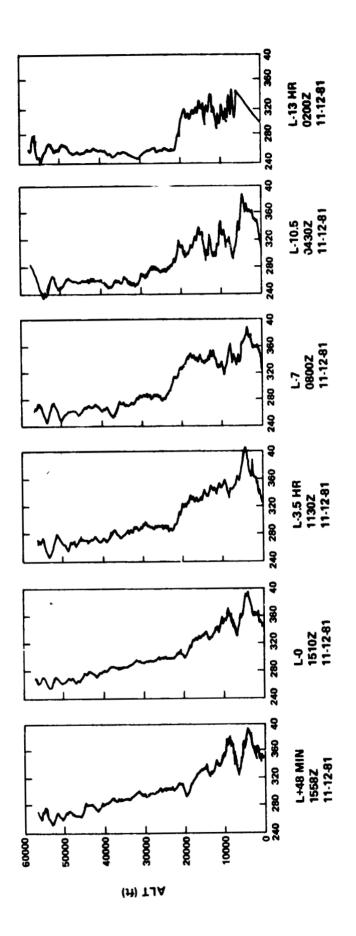
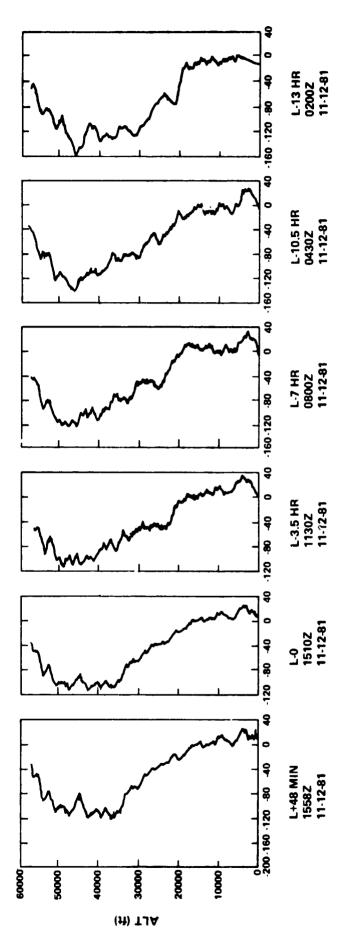


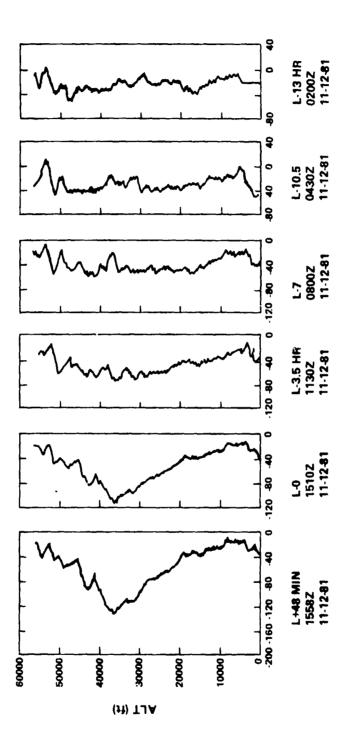
Figure 7. STS-2 prelaunch/launch Jimsphere-measured and estimated wind directions (degrees).



STS-2 prelaunch/launch Jimsphere measured and estimated in-plane component winds (FPS). Flight azimuth = 60 degrees. Figure 8.

40

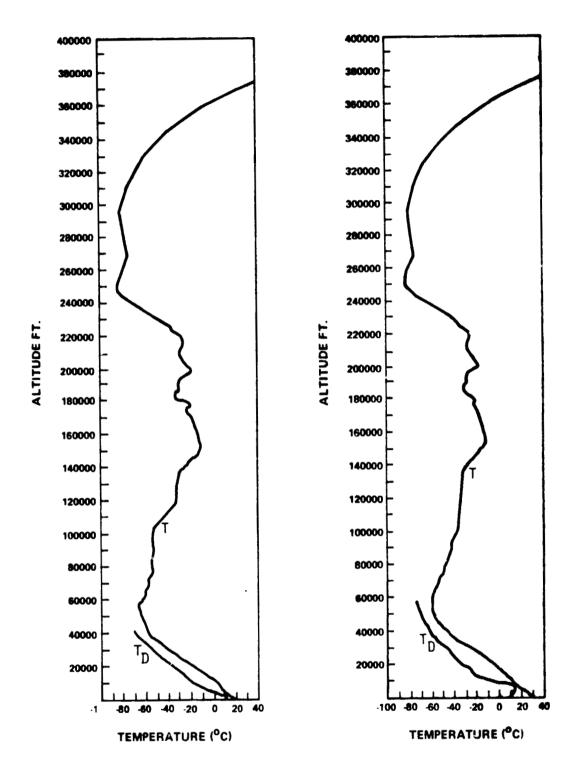
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STS-2 prelaunch/launch Jimsphere measured and estimated out-of plane component winds (FPS). Flight azimuth = 60 degrees. Figure 9.

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 ${\bf T}_{\bf D}$  - Dew point temperature

T - Temperature

Figure 10. STS-2 temperature profiles versus altitude for launch (left) and SRB descent (right).

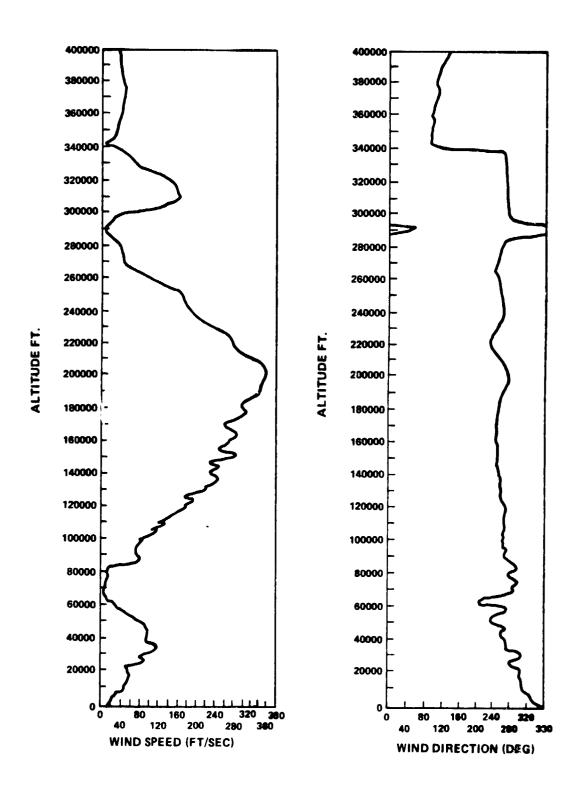


Figure 11. STS-2 scalar wind speed and direction for SRB descent.

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## **APPROVAL**

## ATMOSPHERIC ENVIRONMENT FOR SPACE SHUTTLE (STS-2) LAUNCH

By D. L. Johnson and S. C. Brown

The information in this report has been reviewed for technical content. Review of any information concerning Department of Defense or nuclear energy activities or programs has been made by the MSFC Security Classification Officer. This report, in its entirety, has been determined to be unclassified.

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